

### Application of Global Positioning System (GPS) to Travel Time and Delay Measurements

By

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Summer 2008

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### Introduction

Since 1996, the Global Positioning System (GPS), a worldwide radio-navigation system formed from a constellation of 24 satellites and their ground stations, has collected travel time and delay data on major roadways throughout Delaware. The GPS statistically matches manual data collection in accuracy and is highly efficient and therefore continues to effectively collect data within Delaware today. Every year, a report is compiled documenting and summarizing the collected data. The *Application of Global Positioning System (GPS) to Travel Time and Delay Measurements* – 1997 Phase report describes the testing of the applicability and accuracy of the GPS system, while the 1998 Phase report provides step-by-step instructions for data collection.

In past years, travel data was collected during peak-travel times between mid-September and Thanksgiving. In 2002, data collection expanded to include Summer peak-travel times as well. In 2003, the Summer mileage covered increased from 652 to 896 miles, and in 2004, this mileage increased again from 896 to 1006 miles. In 2008 the mileage increased to 1169 miles. This report describes the methodology used to collect Summer peak-travel time data and includes a summary and conclusion of the collected data.

### Methodology

The continued success of the travel time and delay data collected over the past eleven years in monitoring congestion trends along Delaware roadways in the Fall months has led the Delaware Department of Transportation (DelDOT) to include the major travel routes to and from the shore points during the Summer months in the data collection. This data has become critical to the analysis of travel patterns surrounding the Delaware beaches and to the monitoring of congestion along these major routes.

All major routes leading to and from the Delaware beaches are covered. Routes and numerous additional segments were added in 2003 and even more have been added in 2004. 3 new roads were added in 2008. The new roads are SR 5, Plantation Rd (SR 1D), and SR 30. A small part of SR 30 did exist before. All of the routes covered can generally be divided into two groups:

- North-South roads: SR 1, US 13, US 113, SR 896, SR 71, SR 9, SR 5, SR 30,
   Plantation Rd (SR 1D), 1-95, and I-495. These routes are primarily used by travelers coming to and from the main northern points, including New Castle County,
   Pennsylvania, New Jersey, Cecil County (in Maryland), etc.
- East-West roads: SR 404, SR 14, SR 16, SR 20, SR 24, SR 26, SR 36, SR 54, I-295.
   These roads are generally used by travelers from Maryland, Virginia, and
   Washington, D.C. entering the Delaware shore points.

For each route that was covered, control points were selected between the segments of the roadway. The control points were positioned at major intersections or where road characteristics, such as the number of lanes, speed limit, or development type changed. Once the control points were selected, they were entered into the data dictionary files using the Pathfinder editing system, which allows control points and specific attributes to be added, deleted, or edited. Data dictionary files allow control points and other roadway attributes, such as the speed limit and number of lanes, to be collected and stored with only a click of the mouse.

A major feature that was added to data collection in 2004 was the addition of a background map with corresponding control points to the Aspen software used while driving.

This background map would allow the data collector to view where the car was in relation to the next control point as well as the surrounding roads and intersections. The control points were

represented by red crosses throughout the background map and were placed exactly where the next segment began. Both the background map and control points were added by layering two shape files extracted from the Geographic Information Systems (GIS) network. By adding these features, the data collector no longer had to rely on the car odometer and predetermined distances to anticipate the next control point.

Prior to the start of the project, new equipment was purchased in order to facilitate easier and more accurate data collection. Much of the equipment that had been used in previous years was outdated and not functioning correctly. Two new laptops were purchased, as well as new software, a new antenna, and new cabling for the GPS units. The software upgrade was necessary because the new laptops would not support the older programs. Aspen, which is no longer produced, was replaced by TerraSync, and the GPS Pathfinder Office software was upgraded to version 3.10.

As for data collection times, data was collected on Summer weekends between June 16<sup>th</sup> and August 18<sup>th</sup>. Generally, the majority of beach-goers travel to and from the shore points on Friday afternoons, Sunday afternoons, and throughout the day on Saturday. Traditionally, data has been collected heading toward the beach (southbound and eastbound) on Friday evenings from 3 to 7 PM and from 9 AM to noon on Saturday mornings. Data was also collected heading away from the beach (northbound and westbound) on Saturday evenings from 4 to 8 PM and on Sunday afternoons from 4 to 7 PM.

Due to the better than expected results of the Summer data collection in 2006, the

Delaware Center for Transportation was asked to revise their data collection times to attempt to
capture more of the congestion associated with beach travel. A report entitled *Recommendations*for Revised Methodology for Summer Data Collection Regarding DCT Projects: Applications of

Global Positioning System to Travel Time and Delay was completed in the winter of 2006. The report recommended time intervals in which data collectors should expect to see the most traffic. The report concluded that data collection times for many of the routes should be adjusted on Saturdays in order to collect more accurate data. Data collection times on Friday and Sunday remained the same as the previous year. Appendix A shows the adjusted data collection times; any roads not included in the Appendix A did not need adjustments.

Due to the number of routes to be covered and the need for at least 2 successful runs of each route, it was necessary to use two vehicles to complete the project on time. Two people rode in each car: a driver and a data collector. The latter operated the laptop computer and noted each attribute, while the former attempted to approximate the average driver. While one person might feasibly drive and collect data at the same time, this would present a potential safety hazard.

Each route was driven at least twice in each direction to guarantee the accuracy of the data that was collected. Recommendations for revised Methodology for Summer Data Collection also recommended that SR 1 be completed four times, therefore data for SR 1 was collected four times and data collection was spread as evenly as possible over Friday, Saturday, and Sunday.

In the event of problems, whether due to equipment failure, weekend-long inclement weather, or large irregularities in the travel patterns, the roads were traveled again to ensure that peak beach-traffic patterns were captured. Also, in the event of heavy rain or very poor weather conditions, which did not happen this season, data was not collected at all, in order to avoid the collection of inaccurate data, which would not fully represent particular travel and delay times, as well as ensure the safety of data collectors. Where more than two runs were completed, only

the results of the two or more that best captured the peak volume were used and averaged. Once all the data was collected, exported, and printed, it was analyzed and summarized on a segment-by-segment basis.

### **Differences between Fall and Summer Projects**

The same basic methodology is used in both the Fall and Summer GPS Travel Time projects. In addition, many of the roads covered are the same. However, there are some key differences separating the projects:

- Some of the roads covered during the Summer are different than those covered in the
  Fall. The Fall project emphasizes commuter routes, particularly in New Castle
  County, while the Summer project covers major beach routes throughout the state.
- Instead of weekday morning and afternoon collection times as in the Fall, the Summer data was collected on weekends.
- 3. In the Fall, data is collected separately for both morning (AM) and afternoon (PM), and at least two runs of each route are completed in each direction at each time of day. Results are then tabulated separately for AM and PM. In the Summer, there is no AM/ PM division. Thus, roads are covered only twice in each direction.
- 4. Because the Summer project focuses primarily on statewide, long-distance beach traffic rather than short intra-county commuter trips, the roads are not separated by county as they are in the Fall.

### Interpretation of 2008 Summer Data

This report includes a data table with all of the collected information arranged by route name. The leftmost column contains the name of the route being covered. Each route is then divided into the different segments and data is provided in each direction. To the right of the segment names, the table contains the following information:

- Distance (Miles) This is the distance in miles for the given segment of roadway shown to
  the left. When the term "Total" is specified, the distance corresponds to the total length from
  the first control point to the last.
- Mean Peak Travel Time (Seconds) This is the average time in seconds that was required to travel the length of the segment.
- Mean Peak Travel Speed (mph) The average speed of the test vehicle from one point to the
  next is the Mean Peak Travel Speed. This value is given in miles per hour and is obtained by
  dividing the Distance of the segment by the Mean Peak Travel Time.
- Total Peak Delay (Seconds) This is the time, in seconds, spent in delay on the given segment. By DelDOT's definition, delay is the time during which the vehicle speed drops below five miles per hour.

- Peak Delay Source This is the reason for the delay noted in the previous column. Reasons for delay include signals, construction, accidents, congestion, pedestrian crossings, train crossings, etc. Traffic signals are the primary cause of delay.
- Mean Peak Running Speed (mph) This is the average speed in miles per hour that a vehicle
  would travel through the section of roadway if delay were not experienced. The running
  speed, R, is obtained by the following equation:

$$R = \frac{Distance}{Mean Peak Travel Time - Total Peak Delay}$$

Percent Time in Delay – This is the percentage of time spent in delay for the route segment shown. The percentage is found by dividing the Total Peak Delay by the Mean Peak Travel Time, then multiplying the quantity by 100. Example:

Total Peak Delay = 82.02 sec

Mean Peak Travel Time = 360 sec

Percent Time in Delay = 
$$\frac{82.08 \text{ sec}}{360 \text{sec}} \times 100 = 22.8\%$$

 Number of Lanes – This represents the number of lanes during the given segment. For those segments that have a varying number of lanes, two or more values will appear in this column.  Posted Speed (mph) – This represents the posted speed limit for the given segment of the roadway shown. For segments with more than one posted speed, two or more values will appear in this column.

### **Summary and Conclusions**

Beach traffic congestion during the Summer of 2008 was again collected both precisely and effectively by the GPS Travel Time and Delay project teams. Although 3 new roads received attention, all roads covered in 2007 were again covered in 2008. This allowed for the continuing collection and analysis of travel time and delay time along the existing Summer routes.

Data collection using a GPS unit is an advancement to manual data collection. The system, however, is not perfect and some problems arose. The new equipment eliminated the problems of notebook computers malfunctioning during data collection, which would shut off the GPS units. However, at times the satellite signal was lost, due to inclement weather or tree obstruction. Nonetheless, manual data collection was always feasible and was used in the few instances when necessary.

The results from the 2008 Summer data collection show a general improvement in LOS on almost all routes. Data collection was repeated on some roads due to the lack of congestion the was expected. Interstate 95 and 295 were collected on four separate occasions to try to catch peak traffic flows. During the first times that data was collected on both of the routes, there was little to no congestion. Data was re-collected on these roads during two other different time intervals to try to capture more of the expected congestion.

Data collection teams realized that while traffic was observed to be moderate to heavy on most runs, and speeds were below posted on many roadway segments, vehicles were still moving. Collection teams that were involved in previous years noted that there seemed to be less traffic than the previous year, but the traffic seemed to be more steady throughout the day. It is possible that the extremely high price of gasoline affected some Summer travel. In addition traffic seemed to flow at a more steady volume throughout the entire day on Saturday. It may be possible that travelers are becoming more conscious of traffic delays and therefore spreading their travel out over a longer period of time.

Drivers to the beach appeared to be driving about as fast as in 2007, and drivers were very aggressive on the longer north and south bound roads. Speeds exceeding 70 miles per hour on roads with 55 mph speed limits were not uncommon. In addition, drivers were observed along I-95 and SR 1 driving down the breakdown lane in order to avoid the congestion. Most of the time the drivers on the breakdown lane were trying to turn off onto an exit.

Drivers experienced delays on US 13 in Seaford. Extremely short green times were observed on US 13 at the intersection of Tharp Road. It was observed that only 10-20 vehicles were making it through the green light, and the cross streets had more green time than was needed. In addition, the development of large shopping centers along SR 1 have caused excessive delays near the beach. Drivers appear to be using US 113 to circumvent the signalization along the last few segments of SR 1.

Variability in the time of peak traffic volume also caused difficulties. There are numerous factors that cause variation in this peak time, some of which are current weather, predicted weather, and holidays. If weather is predicted to be poor, fewer vacationers go to the beaches, or if the weather is sunny and then turns rainy, people usually leave early. Even with

the report recommending travel times, those recommended peak times did not always coincide with the peak times on Saturday.

Ideally, in the future, a computerized process to extract the GPS results and travel data is expected to yield greater accuracy and efficiency. Additionally, observations noted that data collection beyond US 13 on the East-West routes, not including SR 404, does not provide strong travel time and delay data and may be unnecessary in future projects. It was determined that hardly any congestion or even volume was observed past this point and up until the Maryland state line. Thus, the last control point on these roads could be placed at the intersections with US 13, as such a change would result in more resources being concentrated on more heavily traveled segments of other routes.

For the most part, data is collected every day of the weekend with no specification given to which day, only which direction. Thus, data collected on Friday evenings is averaged with data collected on Saturday mornings, since both times represent southbound traffic to the shore points. So far, there has been no serious problems or inaccuracies with this method; however, it may be more beneficial to collect and analyze this data on more of a day-to-day basis, with possibly two runs being completed for each route in each direction as well as on each day, in order to allow for a more direct analysis of the data and a more specific account of when beach roads are most congested. However; this may require the addition of one to two more vehicles and teams in order to schedule two runs of each road on each day of the weekend within the given data collection times period.

Also, after careful observation along with direct contact with the toll plazas, as mentioned earlier, it was discovered that congestion northbound on Saturday mornings can be just as high as congestion southbound at this time. Methods of collection including Saturday morning north

bound routes may be a possible addition to future projects, and it may contribute to the accuracy and development of a successful travel time and delay study during the Summer, when traffic peak times do vary considerably. In order to allow for these additions and the time constraints put on Summer data collection, it may be necessary to include a third car, as well as a third set of data collectors, in accomplishing this Summer project in the future. This Summer project was very successful in capturing an accurate picture of travel time and delay all over Delaware and its shore points, and these changes would not only continue the success of the project but allow for a more detailed and comprehensive approach to GPS data collection and its application to such travel time and delay measurements.

Finally, Appendices were attached to this report. Appendix A shows recommended data collection times. Appendix B has 10-most degraded, 10-most improved, and 20-worst segments. Appendix C has a map of the roads covered in Summer 2008. Appendix D describes the methodology of calculating mean peak travel speed. Appendix E describes the methodology of calculating mean peak delay. Appendix F describes the methodology of calculating the difference between posted speed and average speed. Appendices G and H show the Level of services in Summer 2007 and 2008. These appendices are useful to compare the changes in level of service between Summer 2007 and 2008. Appendix I shows the final table containing Summer 2008 data collection data.

### List of Appendices:

Appendix A: Recommended Data Collection Intervals on Saturdays

Appendix B: Notable Segments

Appendix C: Summer Coverage

Appendix D: Mean Peak Travel Speed

Appendix E: Mean Peak Delay

Appendix F: Posted Speed vs. Average Speed Difference

Appendix G: Level of Service 2007

Appendix H: Level of Service 2008

Appendix I: Peak Travel Time Data – Summer 2008

Appendix A

Recommended Data Collection Intervals on Saturdays

Route	Direction	Beginning Segment	Start Time
SR 1	SB	SR 141	9:00–10:00am
	NB	SR 54	4:00-5:00pm
US 113	SB	SR 1 Split	11:00am-12:00pm
	NB	Maryland State Line	4:00-5:00pm
US 13	SB	I-495	9:00–10:00am
(Wilmington to Dover)	NB	SR 1/US 113 Split	4:00-5:00pm
US 13 (Dover to	SB	SR 1/US 13 Split	9:00-10:00am
MD Line)	NB	SR 54	4:00-5:00pm
SR 404	EB	Maryland State Line	10:00-11:00am
	WB	SR 1	4:00-5:00pm
SR 16	EB	Maryland State Line	10:00–11:00am
	WB	SR I	4:00-5:00pm
SR 36	EB	SR 404	10:00–11:00am
	WB	SR 36/16 Split	4:00-5:00pm
SR 20	EB	Maryland State Line	10:00–11:00am
	WB	SR 1	10:00–11:00am
SR 24	EB	Maryland State Line	9:00–11:00am
	WB	SR 1	4:00-5:00pm
SR 26	EB	SR 54 Split	9:00–10:00am
	WB	SR 1	4:00-5:00pm
SR 30	SB	SR 1	10:00-11:00am
	NB	US 13	4:00-5:00pm
SR 1D	SB	US 9	10:00–11:00am
Plantation Rd	NB	SR 1	4:00-5:00pm
SR 5	SB	SR 1	10:00–11:00am
	NB	Indian River Bay	4:00-5:00pm
SR 54	EB	Maryland State Line	9:00–10:00am
	WB	SR 20	4:00-5:00pm

<sup>\*</sup>Routes not included on this chart did not need adjustments in data collection intervals.

<sup>\*</sup>Source: Recommendations for Revised Methodology for Summer Data Collection Regarding DCT Projects: Applications of Global Positioning

System to Travel Time and Delay – Winter 2006

### Appendix B

### Notable Segments:

This is a listing of segments which appear to require special attention:

- 10-Most Degraded Segments
- 10-Most Improved Segments
- 20-Worst Segments

To find these segment the following equations have been used:

$$\%_{PS}$$
  $_{TS} = \frac{Mean\ Peak\ Travel\ Speed\ - Weighted\ Average\ Speed}{Weighted\ Average\ Speed}$ 

$$%_D_PS_TS = %_PS_TS_{2008} - %_PS_TS_{2007}$$

### A<sub>1</sub>: 10-Most Degraded Segments

Segments are selected by taking the difference between the LOS of 2007 and the LOS of 2008 and taking the segments which indicated the most drastic decline. If two or more segments had the same level of degradation, the segment with the least %\_D\_PS\_TS took priority.

### A<sub>2</sub>: 10-Most Improved Segments

Segments are selected by taking the difference between the LOS of 2007 and the LOS of 2008 and taking the segments which indicated the most notable improvement. If two or more segments had the same level of improvement, the segment with the greatest %\_D\_PS\_TS took priority.

### A<sub>3</sub>: 20-Worst Segments

The 20 segments with the greatest LOS are selected and displayed in this table.

A<sub>1</sub>: 10-Most Degraded Segments – 2008:

	Route			LOS	LOS	
ID	Number	Dir	Segment	07	08	%_D_PS_TS
344	SR 24	WB	US 113 to 30/24 split	Α	В	-109.12%
313	SR 20	EB	SR 24 to SR 20 E/US 113 Split	Α	D	-82.90%
160	SR 1	SB	SR 14 to SR 36 (Slaughter Beach)	Α	F	-76.15%
428	SR 54	WB	US 13 to Waller Rd (RD 512)	Α	В	-71.48%
137	SR 1	NB	Exit 97 (two on ramps) to Exit 98	В	F	-68.42%
352	SR 24	EB	SR 5 South to SR 23 / SR 5 North	Α	F	-64.91%
49	US 13 Wilm	SB	SR 273 to US 40	Α	С	-62.50%
13	SR 896	SB	SR 71 to SR 15	Α	В	-56.71%
1	SR 896	SB	I-95 to Old Baltimore Pike	Α	В	-52.23%
175	SR 1	SB	Rehoboth Avenue to King Charles Ave (DE)	Α	Α	-49.93%

### A<sub>2</sub>: 10-Most Improved Segments - 2008:

	Route			LOS	LOS	
ID	Number	Dir	Segment	07	08	%_D_PS_TS
331	SR 24	EB	MD line to Road 499	Α	Α	99.35%
467	l 95	SB	Exit 3 (SR 273) to Exit 1 (SR 896)	D	Α	90.73%
161	SR 1	NB	SR 36 (Slaughter Beach to SR 14)	D	Α	83.92%
463	l 95	NB	Exit 3 (SR 273) to Exit 4 (SR 1)	D	Α	80.36%
469	1 95	NB	MD Line to Exit 1 (SR 896)	С	Α	79.52%
242	SR 404	WB	US 9 Merge to US 113	E	Α	77.25%
464	1 95	SB	Exit 4 (SR 1) to Exit 3 (SR 273)	С	Α	67.14%
290	SR 14	WB	SR 1 to US 113	В	Α	53.64%
5	SR 896	NB	US 40 to Old Baltimore	В	Α	53.20%
248	SR 404	WB	RT 5 to Rt 30	С	Α	52.82%

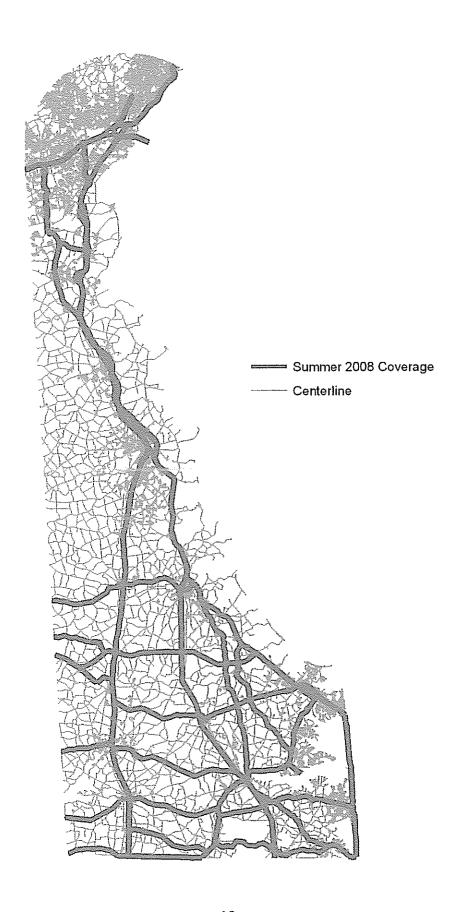
**A<sub>3</sub>: 20-Worst Segments - 2008:** 

	Route					Avg. Speed
ID	Number	Dir	Segment	LOS	LOS %	(mph)
137	SR 1	NB	Exit 97 (two on ramps) to Exit 98	F	80.21%	12.9
101	SR 1	NB	Christiana Mall (exit 164) to Merge with I-95 N	F	79.56%	8.6
160	SR 1	SB	SR 14 to SR 36 (Slaughter Beach)	F	78.49%	11.5
352	SR 24	EB	SR 5 South to SR 23 / SR 5 North	F	74.20%	9.0
23	SR 896	NB	SR 1 to US 13	E	64.88%	8.6
367	SR 26	EΒ	US 113 to SR 20	E	62.32%	10.2
7	SR 896	SB	US 40 to Porter Rd.	E	61.85%	16.0
176	SR 1	NB	King Charles Ave (DE) to Rehoboth Avenue	D	57.74%	13.1
313	SR 20	EB	SR 24 to SR 20 E/US 113 Split	D	56.96%	21.7
235	SR 404	EB	US 13/404 W Split to US 13/404 E Split	D	55.37%	19.6
427	SR 54	EB	Waller Rd (RD 512) to US 13	D	53.64%	11.6
46	US 13 Wilm	SB	SR 141 to SR 273	D	48.27%	19.2
140	SR 1	NB	Combo w/ US 113 (95) to Exit 97 (two on ramps)	D	46.41%	34.8
107	SR 1	NB	US 40 (exit 160) to SR 273 (exit 162)	D	45.42%	29.9
302	SR 20	WB	US 13 / SR 20 E to US 13 / SR 20 W	C	43.87%	21.1
91	US 13 Wilm	SB	US 13/113 Split to 1/113 Merge (SR 1 Exit 95)	C	43.80%	20.4
142	SR 1	SB	Combo w/ US 113 (95) to Exit 93	С	42.61%	27.3
8	SR 896	NB	Porter Rd. to US 40	С	42.01%	24.0
169	SR 1	SB	US 9 West / SR 404 to SR 24	С	41.85%	14.3
397	US 13 Dover	SB	SR 404 W to SR 404 E	С	41.61%	19.8

### Appendix C

### Summer Coverage:

The following GIS drawing displays in red all the routes that are covered by the Summer 2008 GPS data collection.



### Appendix D

### Mean Peak Travel Speed:

The following GIS drawing displays the mean peak travel time in miles per hour in both directions for every segment of the Summer 2008 GPS data collection.

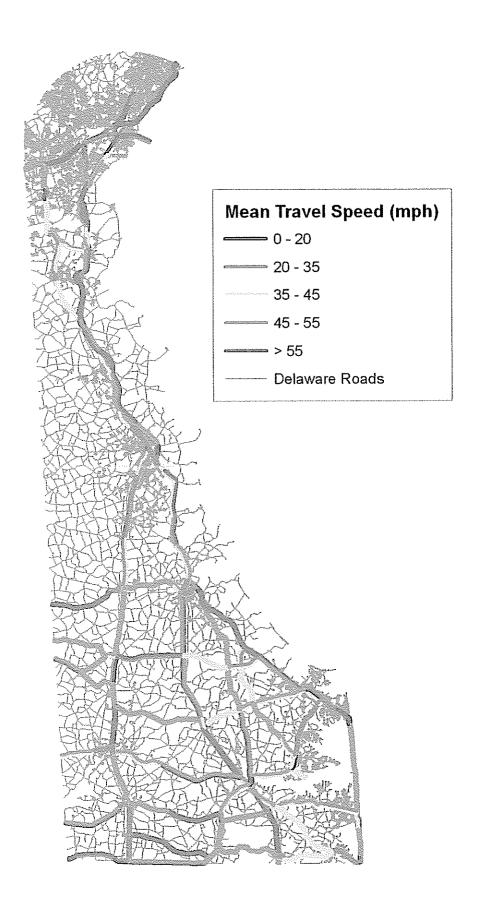
### Methodology:

The mean peak travel speed for every segment is calculated by averaging the total time required to travel the length of each segment of all runs (mean peak travel time), and dividing the segment length by that time.

### **Equations:**

$$MeanPeakTravelTime = \frac{\sum_{1}^{n} TotalTravelTime \_Run(x)}{n}$$

$$MeanPeakTravelSpeed = \frac{SegmentDis \tan ce(Miles)}{MeanPeakTravelTime(Seconds)} * \frac{3600 \sec onds}{1 hour}$$



### Appendix E

### Mean Peak Delay:

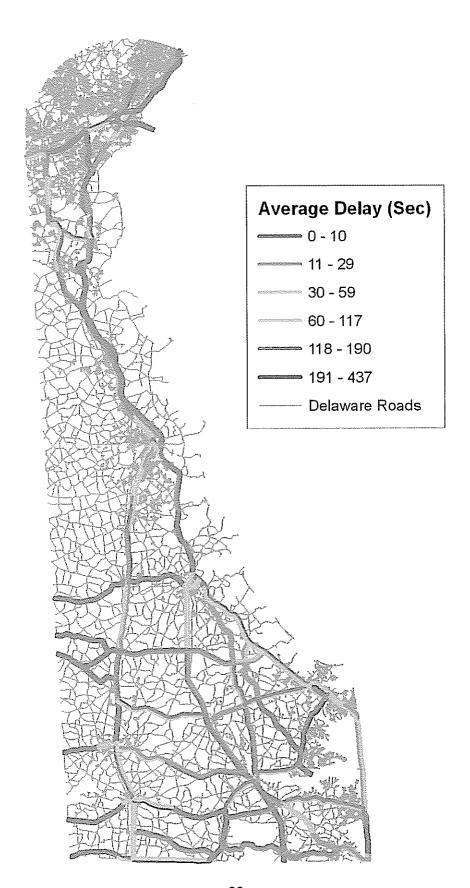
The following GIS drawing displays the average delay along each segment in both directions for every segment of the Summer 2008 GPS data collection.

### Methodology:

Average delay is calculated by adding together the delay measured in each run and dividing the total by the number of runs. The result is displayed in seconds of delay.

### **Equations:**

$$AverageDelay(seconds) = \frac{\sum_{1}^{n} Delay(seconds) \_run(x)}{n}$$



### Appendix F

### Posted Speed vs. Average Speed Difference:

The following GIS drawing displays the percent difference between the posted speed and the average speed for every segment of the Summer 2008 GPS data collection.

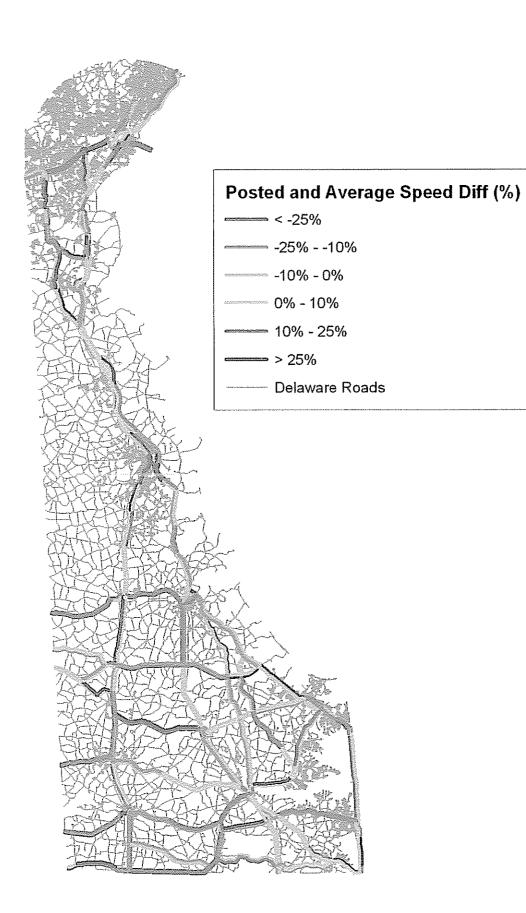
### Methodology:

The percent difference between the posted speed and the average speed is calculated be subtracting the average speed of all runs from the posted speed and dividing the difference by the posted speed. This is done for all segments.

### **Equations:**

Average Speed 
$$=$$
 
$$\frac{\sum_{1}^{n} Average Speed \_run(x)}{n}$$

Posted & Average Speed Diff.% = 
$$\frac{(Posted\ Speed-Average\ Speed)}{Posted\ Speed}*100\%$$



### Appendix G

### Level of Service 2007:

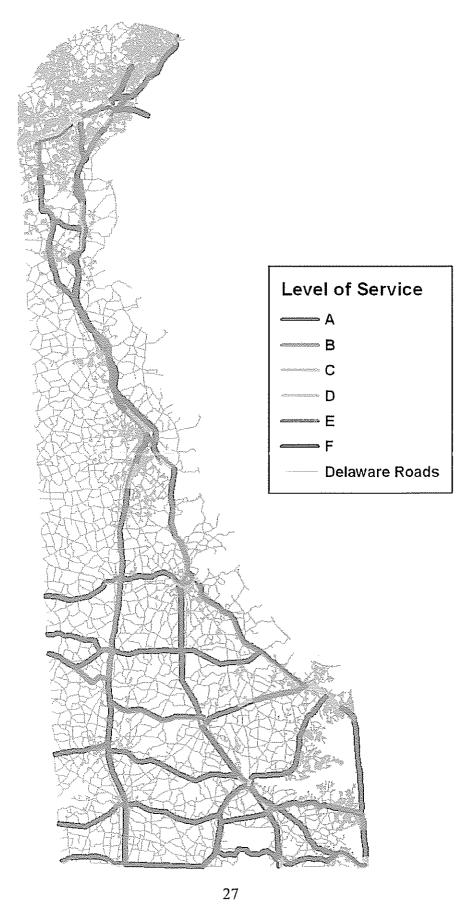
The following GIS drawing displays the calculated level of service for each direction of all segments for every segment of the Summer 2007 GPS data collection.

### Methodology:

Using the percent difference between the posted speed and average speed, the level of service is calculated. By first identifying segments that are interstates or interstate/freeways and roads that are arterials in 2007, the following tables are used to classify the appropriate level of service.

### Percentage of speed below the posted speed limit:

For Interstate or Interstate/Freeways:	Arterials:
LOS A: 0-14%	LOS A: 0-10%
LOS B: 14-18%	LOS B: 10-30%
LOS C: 18-20%	LOS C: 30-45%
LOS D: 20-30%	LOS D: 45-60%
LOS E: 30-50%	LOS E: 60-70%
LOS F: 50% +	LOS F: 70% +



### Appendix H

### Level of Service 2008:

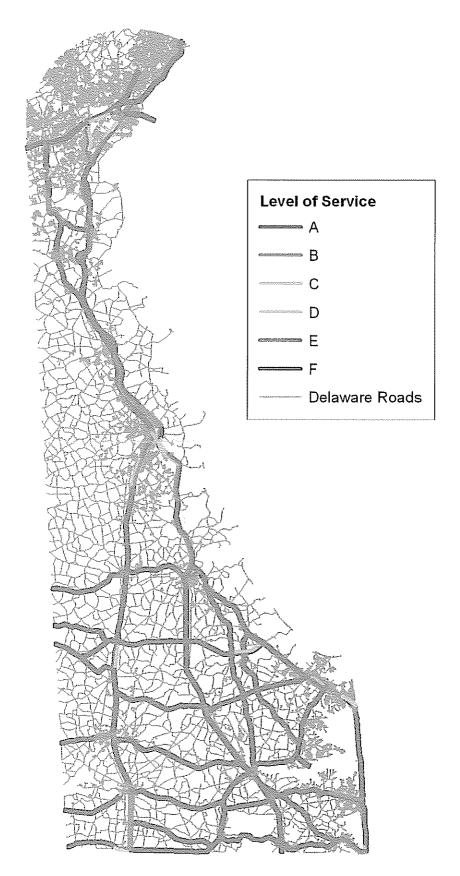
The following GIS drawing displays the calculated level of service for each direction of all segments for every segment of the Summer 2008 GPS data collection.

### Methodology:

Using the percent difference between the posted speed and average speed, the level of service is calculated. By first identifying segments that are interstates or interstate/freeways and roads that are arterials in 2008, the following tables are used to classify the appropriate level of service.

### Percentage of speed below the posted speed limit:

For Interstate or Interstate/Freeways:	Arterials:
LOS A: 0-14%	LOS A: 0-10%
LOS B: 14-18%	LOS B: 10-30%
LOS C: 18-20%	LOS C: 30-45%
LOS D: 20-30%	LOS D: 45-60%
LOS E: 30-50%	LOS E: 60-70%
LOS F: 50% +	LOS F: 70% +



### Appendix I

### Peak Travel Time Data - Summer 2008

The following table is the averaged data for all segments analyzed during the Summer 2008 GPS data collection. The table includes the route number, route name, segment direction, segment distance, mean peak travel time, mean peak travel speed, total delay, peak delay source, mean peak running speed, percent time in delay, number of lanes and the posted speeds.

Comparing to 2007, Mean Peak Travel Speed in the state of Delaware has increased from 42.3 to 43.9 mph. Also Percent Time in Delay has decreased from 15.2% in 2007 to 8.4% in 2008.

The main reason for this improvement could be because of the high price of gas in Summer 2008. In Summer 2008, the national average gas price hit \$4.00/gal. Because the high price of gas, many U.S. families cut some of their summer vacations. This reduction in the number of trips reduced VMT in the Summer 2008 comparing to Summer 2007 and made Delaware roads less congested than what they were in Summer 2007.

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7	Speed	50	50,40		50	50		50,55	55.50		55	25	ů,	200	20	55,50,25	55		25,35,50	50,35,25,55	40.60	90,04	ne				50,35	35,45,50		50,35,25	35,45	25,35,50,40,50,40	50,40,50,35,25				20	50		20	20	7,50	6 2	2
	No. of	2	2		2	7		2.3	2.3		2	2	r	• •	7	2	2		1,2	2.1		4 (	7	-			-	2.1		-	-	-	2.1				2,3	2		3	4.3	76	ψ'; <sub>2</sub>	4
Percent	Time in	39.7%	0.0%		7.1%	18.6%		20.0%	21.2%	-	34.4%	22.9%	700 0	0.2.0	0.070	37.4%	0.0%		17.7%	%0.0	200	80.U	51.0%	22 20%	43 40,	16.1/0	22.2%	1.0%		21.4%	7.9%	0.0%	2.9%		11.7%	3.0%	20.0%	%00		48.3%	40.7%	700 30	9,9°C7	, s
Mean Peak	Kunning Speed (mph)	39.6 39.6	46.5	2.5.	51.1	63.9		20.0	30.4	£	59.4	58.1	7 67	43.9	42.9	53.3	46.4		46.7	48.5	, 44	4,87	17.6	A2 E	46.3	40.4	41.4	41.1		25.9	28.9	42.8	43.6		39.8	40.7	36.8	46.7		35.8	35.2	030	25.9	
Peak	Delay	Source	in the second		Signal	Signal		Road Construction	Signal		Signal	Signal		olgna		Signal	-		Signal	<b>\$</b>			Signal				Signal	Signal	in the control of the	Signal	Signal	***	Signal				Congestion/Signal		**************************************	Congestion/Signal	Congestion/Signal		Congestion/Signal	1
Total Peak	Delay	(Seconds)	9		12	28		64	44		63	38		15	0	87	0		58	0		0	43		340	152	83	3	2	37	11	c	14		121	28	44		>	119	92		62	
Wean Peak	Travel	Speed (mph)	23.3	40.0	47.5	52.0		16.0	24.0		38.9	44.8		40.3	42.9	7 26	46.4		38.4	48.5		29.4	8.6	3 6	33.0	40.6	20.0	7.57	40.7	20.4	25.6	# C7	42.4		35.1	39.5	29.5	200	40.7	18.5	20.9		19.2	
Moan Deak		(S)	1	90	163	150		320	208		183	164		177	164	100	167		328	260		25	84		1547	1257	375	200	/67	174	134	100	485		1031	916	210	217	136	247	226		241	
	Dist. (Miles)		8.0	0.8	2.2	2.2		1.4	1.4		2.0	2.0		2.0	2.0	,	2.2		3.5	3.5		0.2	0.2		14.2	14.2	7.0	7	3.4	1.0	1.0	7 3	2.7	5	10.1	10.1	a +	0,	1,8	1.3	1.3		1.3	
	ă		SS	92	BS	N N		BS	SB.		SB	æ		SB	BB	- 65	g <u>g</u>		88	2		SB	NB.		SB	SB R	G	9 !	2	BS	82	5	0 2		SB	NB	93	C .	SE SE	SB	82		SB	
THE PARTY OF THE P	Segments		I-95 to Old Baltimore Pike	Old Baltimore Pike to 1-95	Ob Builtenants 15 40	Oth Delitation of the Control of the	US 40 to Dalishore	US 40 to Porter Rd.	Porter Rd. to US 40		Porter Rd. to SR 71	SR 71 to Porter Rd.		SR 71 to SR 15	SR 15 to SR 71	ALL COLUMN TO AN	SR 15 to SR 896 / SR 71 Spir (Boyd's Corner Rd)		SR 896 / SR 71 Split (Boyd's Corner Rd) to US 13	110 43 to SB 806 / SR 71 Shift (Boyd's Corner Rd)		US 13 to 5R 1	SR 1 to US 13		I-95 to SR 1	SR1 to I-95	CI-CIPCO CIT AND A CONTRACTOR CON	886 / 71 Spill (Boyd's Corner Rd) to US 3013pill	US 301Split to 896 / 71 Split (Boyd's Corner Rd)	US 301 Spill to SR 299	SR 299 to US 301 Split		SK 299 to US 13	15 15 GB ST ST	896 / 71 Split (Boyd's Corner Rd) to US 13	US 13 to 896 / 71 Split (Boyd's Corner Rd)	1001-730 E	1 -495 10 1-295	F295 to 1-495	1-295 to SR 141	SR 141 to 1-295	THE REPORT OF THE PROPERTY OF	SR 141 to SR 273	
	Route Name		SR 896	SR 896	000	22 23	2K 880	908 92	SR 896	252.15	898	SR 896		SR 896	SR 896		SR 895	020 020	SR 896	808 00	32 330	SR 896	SR 896		CD ORE Total	JO I Ukai		SR 71	SR 71	SD 71	SR 71		SR 71	SK71		SR 71 Total			DuPont Hwy	DuPont Hww	1		DuPont Hwy	
	Route		SR 896	SR 896	200	222 22	SK 850	208 02	25 896	20000	SP 895	SR 896		SR 896	SR 895		SR 896	080 25	20 908	0000	37,030	SR 896	SR 896		00 00	30 VC		SR 71	SR 71	- CO 7.4	SR 71		SR 71	SR 71		SR 7		US 13 Wilm.	US 13 Wilm.	110 12 Wilm	US 13 Willia.		US 13 Wilm.	

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Posted	Speed	50	10.11	55,53	25,55	65	65,55	***************************************	65,55	65	253	55,65		35	35,55	25 56	55,35	00,00	55	55		55,45,35	55		35,45,55	45, 35	55	55.45	er.cc	55	55	AF 40.25	40,40,55	04,04,50	35,50	35		45	45			45 55	25.54	מריחם
JO ON	Lanes	2,4		4, 2	7	2	2		2	2	2	2		2	2	-	<b>,</b>	*	2	2		2	€2		2	2	2		7	2	3.2		۲, 3		3	3		3	6			ļ	<b>†</b>	2,4
Percent	Time in Delay %	17.5%		38.1%	9.1.20	16.0%	11.6%		6.7%	9.4%	5 7%	0.0%		5.9%	10.9%	100	7 60	4.076	1.8%	%00		13.8%	0.0%		13.5%	7.1%	40 1%	7 00/	0/.5.7	13.5%	4.3%	100	15.4%	23.378	36.5%	12.9%		19.4%	7.4%	16.9%	10.4%	200.0	0.7.0	14.U7a
Mean Peak	Running Speed (mph)	45.7		46.6	43.1	62.0	51.3		60.5	65.4	42.2	42.4		49.6	45.8	-	0.10	20.3	63.2	513		49.0	52.9		42.0	42.8	543	2.07	49.5	48.0	49.8		40.8	36.1	30.1	31.4		25.3	31.3	45.7	46.7		30.2	35.9
Peak	Delay Source	Signal		Congestion/Signal	Signal	Signal	Signal		Signal	Signai	Cinnal	in the second		Signal	Signal			Signal	Signal			Signal	444	***************************************	Signal	Signal	Carrio	Olysia:	Signal	Signal	Signal	The state of the s	Signal	Signal	Signal	Signal		Signal	Signal	1			Congestion/Accident	Cangestion
Total Peak	Delay (Seconds)	17		153	14	28	20		13	18		<u>r</u> c		14	30			19	¥			26	0		21	10		32	27	24	_		55	66	25	5		76	21	729.5	409.6		15	99
Wean Peak	Travel Speed (mph)	37.7		28.8	47.2	52.1	45.4		56.4	59.3	: :	23.0	4.2.4	46.7	40.8		57.6	48.5	1 63	06.1	51.5	42.2	52.9		36.4	39.7		46.7	45.3	41.5	47.7		34.5	29.1	19.1	27.4		20.4	29.0	38.0	41.8		47.1	29.8
Mean Peak	Travel Time	96		401	275	173	170		198	188		544	677	241	277		338	401	244	147	L67	191	151		154	141		311	334	176	153		355	421	68	41		391	281	43490	3920.7		236	386
	Dist. (Miles)	1.0		3.2	3.6	2.5	2.1	-	3.1	3.1	-	7.7	7.7	3.1	3.1		5.4	5.4	-	7.7	4.3	2.2	2.2		1.6	1.6		4.2	4.2	2.0	2.0		3.4	3.4	0.4	0.3	Š	2.2	2.3	L	45.6		3.1	3.2
F	oj.	92		SB	- R	SB	9	2	SB	82		B :	I NR	SB	2		SB	SS.	-	8	SN N	BS	eg 2		SB	SS.		BS B	8	SB	2		SB	BN	as:	E Z	2	SB	NB NB	as,	S an		SB	NB
	Segments	US 40 to SR 273	The state of the s	US 40 to SR 1/13 Merge	SR 1/ US 13 Split to US 40	CD 111C 13 Marrie to SB 72 (152)	SO 1703 13 Weige to 517 1227	37 72 (132) 13 St 103 (25)	SR 72 (151) to C&D Canal	C&D Canal to SR 72 (152)	and the second s	C&D Canal to SR 896	SR 896 to C&D Canal	SR 895 to SR 299	SR 299 to SR 896	**************************************	SR 299 to SR 71	SR 71 to SR 299	THE PARTY OF THE P	SR 71 to SR 1 (ex 119)	SR 1 (ex 119) to SR 71	SR 1 to SR 6E (Commerce St)	SP 6F (Commerce St) to SR 1		SR 6E (Commerce St) to SR 1 (to exit 114)	SR 1 (to exit 114) to SR 6E (Commerce St)	11.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1	SR 1 (to exit 114) to SR 42	SR 42 to SR 1 (to exit 114)	SB 43 in Scarbotouph Bd	Scarborough Rd to SR 42	***************************************	Scarborough Rd to SR 8	SR 8 to Scarborugh Rd	CD B 10 13 Calia	27. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	ס עס הואלואלי ואי ס	US 13/113 Split to 1/113 Merge (SR 1 Exit 95)	1/113 Split (SR 1 Exit 95) to US 13/113 Merge	1 KA 1 4 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1-495 OVerpass to 1/113 Spint	1113 Opin to 1433 Overpass	SR 141 to Merge with SR 1	Merge with I-95 N to SR 141
	Route Name	DuPont Hwy		DuPont Hwy	DuPont Hwy		DuPont rawy	DuPont Hwy	DuPont Hwy	DuPont Hwy		DuPont Hwy	DuPont Hwy	Dadon Han	DuPant Hwy		DuPont Hwy	DuPont Hwy		DuPant Hwy	DuPont Hwy	DuPont Hwy	Concern Tay	Durdin nwy	DaPont Hwy	DuPont Hwy		DuPont Hwy	DuPont Hwy	Control Control			DuPont Hwy	DuPant Hwy			DuPont Hwy		US 113		US 13 Wilm. Total		56-1	1.95
	Route	US 13 Wilm			US 13 Wilm.	-		US 13 Wilm.	US 13 Wilm	-		US 13 Wilm.		11C 52 Million			US 13 Wilm.	ш	ŀ	US 13 Wilm.	US 13 Wilm.	11S 13 Wilm	15 43 William	US 13 WILLS.	11S 13 Wilm	US 13 Wilm.		US 13 Wilm.	US 13 Wilm.	15 42 1461-	US 13 WILL.	2.00	US 13 Wilm.	US 13 Wilm.	104.00	US 13 WEITH.	US 13 Wilm.	11S 13 Wilm	US 13 Wilm.		US 13 W		SR 1	SR 1

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Route	Route Name	Segments	ż	Dist. (Miles)	Mean Peak Travel Time	Mean Peak Travel	Delay	Delay	Running	Time in	No. of Lanes	Posted Speed	e e
					(Seconds)	Speed (mpn)	(seconds)	aningo	dudud paads	w faming			
SR 1	SR1	Merce with SR 1 to Christiana Mall (exit 164)	SB	1	100	38.2	0		38.2	0.0%	2	55	ပ
SR1	SR 1	Christiana Mall (exit 164) to Merge with I-95 N	NB.	0.5	207	8.6	23	Congestion	1.6	11.0%	2	50,45	u.
								WWW		, ou v	-	43	٥
SR 1	SR 1	Christiana Mall (exit 164) to SR 273 (exit 162)	SB	6.0	48	69.5	0	AUTHORITON PROPERTY AND A LABORATORY AND A STATE OF THE AUTHORITON	C'RO	20.0	7,	25 25	c (
SR1	SR 1	SR 273 (exit 162) to Christiana Mall (exit 164)	2	0.9	88	32.7	6	Сопдеянов	\$0.3	8.5%	7	33,30	,
00	1 92	SR 273 (exit 162) to US 40 (exit 160)	SB	1.7	125	50.1	-	Congestion	50.5	0.8%	2	55	A
t as	500	11S 40 (exit 160) to SR 273 (exit 162)	SN SN	1.7	208	29.9	-	Congestion	30.0	0.3%	2	55	۵
No.	45	(20. 100) 0 (20. 100) 0 (20. 100)	<u>!</u>		<b>T</b>			THE PARTY OF THE P					
SR 1	SR 1	US 40 (exit 160) to US 13 North (exit 156)	쭚	1.7	120	50.1	to.	Congestion	51.5	2.6%	2	55	¥
SR 1	SR 1	US 13 North (exit 156) to US 40 (exit 160)	88 88	2.3	171	48.1	0	Congestion	48.1	0.0%	3,2	55	6
		The state of the s	-	ť		* 03			59.4	%0.0		65	¥
SR 1	SR 1	US 13 North (exit 155) to SR 72 (exit 152)	8 2	2.3	130	58.7	0	Condestion	58.7	0.0%	3	65,55	A
SK3	SR1	SK /2 (EXI 132) IO O3 13 NOTH (EXIL 130)		*				The state of the s					
58 t	SR1	SR 72 (exit 152) to C&D Canal	SB	2.8	186	54.1	2	Congestion	54.7	1.1%	3	65	В
SR 1	SR 1	C&D Canal to SR 72 (exit 152)	g.	3.0	161	66.6	0	***	66.6	0.0%	2,3	65	4
										700			
SR 1	SR 1	C&D Canal to SR 696 (exit 142)	SB	3.0	217	49.6	75	Toll Plaza	76.0	34.7%	3.2	65	<u>ر</u>
SR 1	SR 1	SR 896 (exit 142) to C&D Canal	8	2.8	139	72.4	0	Toll Cangestion	72.4	0.0%	2 1	62	4
		AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA								, o ac	-	u	
SR 1	SR1	SR 896 (exit 142) to SR 299 (exit 135)	es S	3.9	218	65.1	7	Cangestian	03.0	0,0%		30 2	- a
SR 1	SR 1	SR 299 (exit 135) to SR 896 (exit 142)	2	3.9	245	57.8	0		97.9	0.0%		50	2
į	- 444	100 tival (15 tival and	a.	9.6	055	62.9	3	Conqestion	63.3	0.6%	2	65	A
ראה המי	- 50	10 20 (CAN 100 ) (CAN 100) (CAN 100)	9	96	489	70.5	10	***	72.0	2.0%	2	65	٧
בה בה	- No	00 (2) (4) (1) (0) (2) (2) (2) (2)	2	?;	22.			The same with the same statement of the same					
SR	58.1	US 13 South (exit 119) to US 13-Smyrna (exit 114)	SB	4.0	215	67.4	0		67.4	0.0%	2	65	¥
SR 1	SR 1	US 13-Smyma (exit 114) to US 13 South (exit 119)	BB.	4.1		67.4	0		67.4	%0.0	2	65	¥
								***************************************	-		-	2.4	c
SR 1	SR 1	US 13-Smyrna (114) to Scarborough Rd (104)	SB	6.3	491	46.2	0	**	46.2	0.0%	7 5	00 10	n <
SR 1	SR 1	Scarborough Rd (104) to US 13-Smyrna (114)	뫼	6.3	332	68.6	0	Congestion	68.6	0.0%	7 7	60	
	F G G	Crathornich B4 (104) to Evit 08	a.	3.0	408	34.3	150	Toll Conqestion	54.3	36.9%	2,4,2	65	63
- 65 - 65	SE	Exit 98 to Scarborough Rd (104)	2	3.9	286	48.9	-	Cangestion/Toll Cangestion	49.0	0.2%	2,4,2	65	æ
		***************************************										4.4	
SR 1	SR 1	Exit 98 to Exit 97 (two on-ramps)	SB	1.2	63	67.6	0		67.6	0.0%		n n	۱
SR 1	SR 1	Exit 97 (two on ramps) to Exit 98	SB		327	12.9	0	Congestion	12.9	0.0%	7	co	
, 45	* 00	# 11 07 thus an enterty to Company 115 113 (05)	u U	Ľ	101	48.4	53	Conqestion	68.3	29.1%	2	55	4
70	י אס	(col oct too wooding) to find own (college)	2 07	:	CPS	348	0	Congestion	34.8	0.0%	2	65	۵
SK1	SR 1	Combo W/ US 113 (95) (0 Ext 9/ (W0 on lamps)	2	_	76.	0.15							
SR 1	SR 1	Cambo w/ US 113 (95) to Exit 93	SB	1.0	128	27.3	17	Cangestion	31.6	13.4%	2,3	55	0
SR 1	SR 1	Exit 93 to Combo w/ US 113 (95)	8 B	Ē	85	41.1	0	Congestion	41.1	0.0%	3.2	55,65	
		And determinents the state of t									,		,
SR 1	SR 1	Exit 93 to SR 9	SB	1.7	162	37.1	3	Congestion	37.7	1.7%	3,2	22	ა -
SR 1	SR 1	SR 9 to Ext 93	82		106	57.0	0		57.0	0.0%	2	52	Α.
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46.1         87         Signal         54.1         14.8%         2           57.3         59         Signal         65.3         12.3%         2           61.0         4         Signal         61.5         0.8%         2           52.9         16         Construction/Signal         54.6         3.0%         2           46.2         1         Signal         46.7         1.1%         2           44.6         0         -         -         44.6         0.0%         2	87         Signal         54.1         14.8%           59         Signal         65.3         12.3%           4         Signal         61.5         0.8%           16         Construction/Signal         46.7         1.1%           0         -         44.6         0.0%           0         -         44.6         0.0%           22         Signal         59.5         4.8%	87         Signal         54.1         14.8%           59         Signal         65.3         12.3%           4         Signal         61.5         0.8%           16         Construction/Signal         54.6         3.0%           0         -         44.6         0.0%           0         -         59.5         0.0%           22         Signal         59.5         4.8%           19         Signal         49.0         14.4%	Signal         54.1         14.8%           Signal         65.3         12.3%           Signal         61.5         0.8%           Construction/Signal         54.6         3.0%           -         46.7         1.1%           -         59.5         0.0%           Signal         59.5         4.6%           Signal         59.5         4.6%           Signal         59.5         4.6%           Signal         49.0         14.4%           -         52.3         0.0%	Signal         54.1         14.8%           Signal         65.3         12.3%           Signal         61.5         0.8%           Construction/Signal         46.7         1.1%           -         44.6         0.0%           Signal         49.0         14.4%           Signal         49.0         14.4%           Signal         49.0         14.4%           -         59.5         0.0%           -         52.3         0.0%           -         48.6         0.0%	Signal         54.1         14.8%           Signal         65.3         12.3%           Signal         61.5         0.8%           Construction/Signal         46.7         1.1%           -         44.6         0.0%           Signal         59.5         0.0%           Signal         48.0         14.4%           Signal         48.6         0.0%           -         48.6         0.0%	Signal         54.1         14.8%           Signal         65.3         12.3%           Signal         61.5         0.8%           Construction/Signal         46.7         1.1%           -         44.6         0.0%           Signal         49.0         14.4%           Signal         49.0         14.4%           -         52.3         0.0%           -         48.6         0.0%           -         48.6         0.0%           -         48.6         0.0%           -         56.7         0.0%           -         56.7         0.0%           -         56.7         0.0%           -         56.7         0.0%	Signal         54.1         14.8%           Signal         65.3         12.3%           Signal         61.5         0.8%           Construction/Signal         46.7         1.1%           -         59.5         0.0%           Signal         49.0         14.4%           Signal         49.0         14.4%           -         52.3         0.0%           -         46.1         0.0%           -         52.3         0.0%           -         55.7         0.0%           -         56.7         0.0%           -         58.7         0.0%           -         58.9         0.0%	Signal         54.1         14.8%           Signal         65.3         12.3%           Signal         61.5         0.8%           Construction/Signal         46.7         1.1%           Signal         44.6         0.0%           Signal         49.0         14.4%           Signal         48.6         0.0%           -         46.7         1.0%           -         59.5         0.0%           -         46.0         0.0%           -         46.1         0.0%           -         46.1         0.0%           -         46.1         0.0%           -         55.3         0.0%           -         56.7         0.0%           -         58.9         0.0%           -         58.9         0.0%           -         58.6         1.0%	Signal 54.1 14.8% 12.3%	Signal         54.1         14.8%           Signal         65.3         12.3%           Signal         61.5         0.8%           -         46.7         1.1%           Signal         46.7         1.1%           Signal         49.0         14.4%           Signal         49.0         14.4%           -         52.3         0.0%           -         48.6         0.0%           -         56.7         0.0%           -         56.7         0.0%           -         58.9         0.0%           -         58.6         1.0%           -         58.6         1.0%           -         52.5         0.0%           -         52.5         0.0%           -         52.5         0.0%           -         52.5         0.0%           -         52.5         0.0%	Signal 54.1 14.8%   12.3%   12	Signal         54.1         14.8%           Signal         65.3         12.3%           Signal         61.5         0.8%           Signal         46.7         1.1%           Signal         44.6         0.0%           Signal         49.0         14.4%           Signal         49.0         14.4%           Signal         59.5         0.0%           -         52.3         0.0%           -         55.7         0.0%           Signal         58.6         1.0%           -         58.9         0.0%           -         52.5         0.0%           -         52.5         0.0%           -         56.7         10.0%           -         58.6         1.0%           -         56.3         6.4%           -         56.3         6.4%	Signal         54.1         14.8%           Signal         65.3         12.3%           Construction/Signal         61.5         0.8%           Signal         46.7         1.1%           Signal         46.7         1.1%           Signal         59.5         4.6%           Signal         48.6         0.0%           Signal         58.5         0.0%           Signal         58.9         0.0%           Signal         58.3         6.4%           Signal         58.3         6.4%           Signal         58.3         6.4%	Signal         54.1         14.8%           Signal         65.3         12.3%           Signal         61.5         0.8%           Construction/Signal         54.6         3.0%           Signal         46.7         1.1%           Signal         46.7         1.1%           Signal         48.6         0.0%           -         58.3         0.0%           -         56.7         0.0%           Signal         58.9         0.0%           -         56.7         0.0%           -         58.9         0.0%           -         58.9         0.0%           -         58.5         0.0%           -         58.6         1.0%           -         56.3         6.4%           -         55.7         0.0%           -         56.3         6.4%	Signal         54.1         14.8%           Signal         65.3         12.3%           Construction/Signal         61.5         0.8%           Signal         46.7         1.1%           Signal         46.7         1.1%           Signal         48.6         0.0%           Signal         48.6         0.0%           Signal         58.5         4.6%           Signal         58.9         0.0%           Signal         58.9         0.0%           Signal         58.9         0.0%           Signal         58.9         0.0%           Signal         58.0         0.0%           Signal         58.5         0.0%           Signal         58.5         0.0%           Signal         58.5         0.0%           Signal         58.5         0.0%           Signal         52.5         0.0%           Signal<	54.1     14.8%       65.3     12.3%       65.3     12.3%       65.3     12.3%       54.6     3.0%       54.6     3.0%       44.6     0.0%       49.0     14.4%       48.1     0.0%       52.3     0.0%       48.6     0.0%       52.3     0.0%       56.7     0.0%       56.7     0.0%       58.9     1.0%       56.3     6.4%       55.7     0.0%       55.7     0.0%       55.7     0.0%       52.5     3.5%       52.5     3.5%       52.5     3.5%       52.5     3.5%       52.5     3.5%       52.5     3.5%       52.5     3.5%       52.5     3.5%       52.5     3.5%       52.5     3.5%       52.5     3.5%       52.5     3.5%       52.5     3.5%       52.5     3.5%	54.1     14.8%       65.3     12.3%       65.3     12.3%       54.6     3.0%       54.6     3.0%       46.7     1.1%       44.6     0.0%       59.5     0.0%       48.0     14.4%       48.1     0.0%       56.7     10.0%       56.7     10.0%       56.3     6.4%       56.3     6.4%       56.3     6.4%       56.3     0.0%       55.3     0.0%       56.3     6.4%       56.3     6.4%       55.3     10.0%       55.3     10.0%       56.3     6.4%       56.3     6.4%       51.8     0.9%       51.8     0.9%       51.8     0.9%       51.8     0.0%       51.8     0.0%	54.1     14.8%       65.3     12.3%       65.3     12.3%       61.5     0.8%       54.6     3.0%       54.6     3.0%       44.6     0.0%       59.5     0.0%       59.5     0.0%       52.3     0.0%       52.3     0.0%       52.3     0.0%       56.7     0.0%       56.3     6.4%       56.3     6.4%       56.3     6.4%       56.3     6.4%       56.3     0.0%       55.3     10.2%       1     50.2     0.4%       51.8     0.9%       47.9     10.2%       57.2     10.2%	54.1     14.8%       65.3     12.3%       65.3     12.3%       65.3     12.3%       54.6     3.0%       54.6     3.0%       44.6     0.0%       44.6     0.0%       59.5     0.0%       48.6     0.0%       52.3     0.0%       56.7     0.0%       56.7     0.0%       56.3     7.1%       56.3     0.0%       56.3     0.0%       55.3     0.0%       56.3     0.0%       56.3     0.0%       56.3     0.0%       55.3     10.0%       55.3     10.0%       55.3     10.0%       52.5     0.0%       52.5     0.0%       52.5     0.0%       52.5     0.0%       52.5     0.0%       52.5     0.0%       52.5     0.0%       52.5     0.0%       52.5     0.0%       52.5     0.0%       52.5     0.0%       52.5     0.0%       6.0     0.0%       7.2     0.0%       8.2     0.0%       8.2     0.0%       9.2     0.0%	54.1         14.8%           65.3         12.3%           65.3         12.3%           65.3         12.3%           54.6         3.0%           54.6         3.0%           46.7         1.1%           44.6         0.0%           59.5         0.0%           48.0         14.4%           48.1         0.0%           58.3         0.0%           56.7         10.0%           56.7         10.0%           56.3         6.4%           56.3         6.4%           56.3         6.4%           56.3         0.0%           55.3         10.0%           56.3         6.4%           56.3         6.4%           56.3         6.4%           56.3         6.4%           57.2         10.2%           57.2         10.2%           57.2         0.0%           52.4         0.0%           52.4         0.0%           52.4         0.0%	54.1     14.8%       65.3     12.3%       65.3     12.3%       65.3     12.3%       54.6     3.0%       54.6     3.0%       54.6     3.0%       55.5     0.0%       44.6     0.0%       59.5     0.0%       48.6     0.0%       52.3     0.0%       53.1     10.9%       56.7     0.0%       56.3     7.1%       56.3     0.0%       56.3     0.0%       55.7     0.0%       55.7     0.0%       55.7     0.0%       55.3     10.2%       57.2     10.2%       47.9     10.2%       52.4     0.0%       52.5     3.5%       6.4%     0.0%       55.7     0.0%       55.7     0.0%       55.3     10.2%       52.4     0.0%       52.4     0.0%       52.5     30.4%
41 Signal   43.3	41 Signal 43.3   43.3	41   Signal   43.3	Signal   43.3	Signal   43.3	Signal   43.3     Signal   54.1     Signal   65.3     Signal   61.5     Signal   44.6     Signal   49.0     Signal   49.0     Signal   49.0     Signal   49.0     Signal   49.0     Signal   48.6     The state of	Signal   43.3	Signal   43.3	Signal   43.3     Signal   65.3     Signal   61.5     Signal   44.6     Signal   49.0     Signal   48.6     -	Signal   43.3	Signal   43.3     Signal   65.3     Signal   61.5     Signal   64.6     Signal   44.6     Signal   49.0     Signal   48.6     - 46.1     Signal   58.5     - 58.3     - 58.5     - 58.7     Signal   58.6     - 58.7     Signal   58.6     - 58.7     Signal   58.6     Signal   56.7     Signal   56.7     Signal   56.7	Signal 65.3   54.1   54.5   54.1   54.5   54	Signal   43.3   Signal   54.1   54.6	Signal   43.3     Signal   65.3     Signal   61.5     Signal   44.6     Signal   48.0     Signal   58.5     Signal   58.5     Signal   58.7     Signal   58.7     Signal   56.7     Signal   56.3     Signal   56.7     Signal   56.3     Signal   56.3     Signal   55.7     Signal   5	Signal   43.3     Signal   54.1     Signal   65.3     Signal   61.5     Signal   46.7     Signal   49.0     Signal   48.6     Signal   59.5     Signal   59.5     Signal   58.9     Signal   58.0     Signal   58.0     Signal   58.0     Signal   58.0     Signal   58.5     Signal   58.7     Signal   55.3     Construction/Signal   52.5	Signal   43.3	65.3 66.3 61.5 61.5 64.6 64.6 64.6 64.6 64.6 64.6 64.6 65.7 65.7 65.7 65.3 65.3 65.7 65.3 65.7 65.3 65.7 65.3 65.7 65.3 65.7 65.7 65.3 65.7 65.7 65.7 65.7 65.7 65.7 65.7 65.7	54.1 65.3 65.3 61.5 54.6 61.5 54.6 61.5 44.6 44.6 44.6 48.6 62.3 55.7 56.3 56.3 56.3 56.3 56.3 56.3 56.3 56.3	54.1 65.3 65.3 65.3 61.5 54.6 64.6 44.6 44.6 46.7 48.0 59.5 59.5 59.5 58.9 58.9 58.9 58.0 58.0 58.0 58.0 58.0 58.0 58.0 58.0	54.1 65.3 65.3 61.5 54.6 64.6 64.6 64.6 64.6 64.6 64.6 64	54.1 65.3 65.3 65.3 61.5 54.6 61.5 54.6 61.5 64.6 44.6 44.6 44.6 48.6 62.3 56.7 56.3 56.3 56.3 56.3 56.3 56.3 56.3 57.2 57.2 57.2 57.2	54.1 65.3 65.3 65.3 61.5 54.6 64.5 64.6 64.5 59.5 59.5 59.5 59.5 58.9 58.9 58.0 58.0 58.0 58.0 58.0 58.0 58.0 58.0
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	φ w 4 4 w w	61.0 52.9 46.2 59.5 59.5 41.9	61.0 52.9 46.2 44.6 59.5 56.7 41.9	52.9 52.9 44.6 44.6 59.5 56.7 41.9 46.1	61.0 44.6 44.6 52.9 56.7 56.7 66.7 46.1	61.0 52.9 46.2 44.6 59.5 56.7 56.7 41.9 62.3 66.1 46.1 48.6	52.9 46.2 44.6 44.6 56.7 56.7 52.3 52.3 52.3 48.6 47.3	52.9 44.6 44.6 59.5 56.7 52.3 52.3 46.1 46.1 46.1 46.1 46.1 46.1 46.1 46.1	52.9 44.6 44.6 44.6 59.5 56.7 52.3 58.0 58.0 53.5 54.0												
NB 8.0 543 SB 1.2 92 NB 1.2 94	8.0 1.2 1.2 7.1 7.1	8.0 1.2 1.2 7.1 7.1 7.1	8.0 1.2 1.2 7.1 7.1 7.1 1.5	8.0 1.2 1.2 7.1 7.1 7.1 1.5 1.5	8.0 1.2 1.2 7.1 7.1 7.1 1.5 1.6 1.6	1.2 1.2 1.2 7.1 7.1 7.1 1.5 1.6 1.6 1.6 1.6 1.6 1.6 2.0	1.2 1.2 7.1 7.1 7.1 7.1 1.5 1.6 1.6 1.6 1.6 1.6	8.0 1.2 1.2 7.1 7.1 7.1 1.5 1.5 1.6 1.6 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	1.2 1.2 1.2 7.1 7.1 7.1 7.1 1.5 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6	1.2 1.2 1.2 7.1 7.1 7.1 7.1 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1	1.2 1.2 1.2 1.2 7.1 1.5 1.5 1.5 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6	1.2   1.2   7.1	1.2   1.2   1.2   1.2   1.2   1.2   1.5	8.0 1.2 1.2 1.1 7.1 1.5 1.5 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6	1.2 1.2 1.1 7.1 7.1 7.1 7.1 1.5 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6	8.0 1.2 1.2 1.2 1.5 1.5 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6	1.2   1.2   1.2   1.2   1.2   1.5	1.2 1.2 1.2 7.1 7.1 7.1 1.5 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6	1.2 1.2 1.2 1.2 1.5 1.5 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6	1.2   1.2   1.2   1.2   1.2   1.2   1.2   1.5	8.0 1.2 1.2 1.1 1.5 1.5 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6
SR 404/18 to US 9 (non truck raute) SB 1.2 US 9 (non truck raute) to SR 404/18 NB 1.2	88 NB SB NB	88 88 88	88 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	88 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	88 BN BS BN BN BN BS BN	88 BN	88 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	88 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	88 88 88 88 88 88 88 88 88 88 88 88 88		88 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	88     <	88     <	88       88 <td>88     &lt;</td> <td>88       88   <td>88 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8</td><td>88       88   <td>88 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8</td><td>88       88   </td></td></td>	88     <	88       88 <td>88 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8</td> <td>88       88   <td>88 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8</td><td>88       88   </td></td>	88 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	88       88 <td>88 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8</td> <td>88       88   </td>	88 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	88       88
	SB 7.1 NB 7.1	SB 7.1 NB 7.1 SB 1.5	SB 7.1 NB 7.1 NB 7.1 NB 1.5 NB	SB 7.1 NB 7.1 NB 7.1 NB 1.5 NB 1.5 NB 1.5 NB 1.5 NB 1.5 NB 1.6 NB	SB 7.1 SB 7.1 SB 1.5 SB 1.5 SB 1.6 SB	SB 7.1 SB 7.1 SB 1.5 SB 1.6 SB	SB 7.1 NB 7.1 NB 1.5 NB 1.6 NB 2.0 NB 2.0 SB 5.8 SB 5.8	SB 7.1 NB 7.1 NB 1.5 NB 1.5 NB 1.6 NB 1.6 NB 1.6 NB 1.6 NB 1.6 NB 1.6 NB 2.0 NB 2.0 NB 2.0 NB 5.7 NB	SB 7.1 NB 7.1 NB 1.5 NB 1.5 NB 1.6 NB	SB 7.1 NB 7.1 NB 7.1 NB 1.5 NB 1.6 NB	SB 1.5   NB 1.6   NB 1.6   NB 1.6   NB 1.6   NB 1.6   NB 1.6   NB 1.0   NB	SB 1.5   SB 1.6   SB	SB 1.5   NB 1.5   NB 1.6   NB	SB 1.5 NB 1.5 NB 1.6 NB	SB 7.1  SB 1.5  NB 1.6  NB 1.6  NB 2.0  NB 2.0  NB 2.0  NB 2.0  NB 2.0  NB 2.0  NB 3.7  SB 68	NB   7.1   NB   7.1   NB   7.1   NB   1.5   NB   1.6   NB   1.6   NB   2.0   NB   2.0   NB   2.0   NB   2.0   NB   2.0   NB   3.7   NB   3.3   NB   3.3	SB   7.1   SB   7.1   SB   1.5   SB   1.6   SB   1.6   SB   SD   SD   SD   SD   SD   SD   SD	SB   7.1	NB	SB   7.1   SB   1.5   SB   1.5   SB   1.6   SB   1.6   SB   S.7   SB   SB   S.7   SB   SB   SB   SB   SB   SB   SB   S	NB   7.1   NB   7.1   NB   7.1   NB   1.5   NB   1.6   NB   1.6   NB   1.6   NB   2.0   NB   2.5   NB   2.5

Route	Route Name	Seyments	Ë	Dist. (Miles)	Mean Peak Travel Time (Seconds)	Nean Peak Travel Speed (mph)	Delay (Seconds)	reak Delay Source	Mean reak Running Speed (mph)	Time in Delay %	No. of Lanes	Posted Speed	ros
1							-		907	10 607	-	50	۵
SR 404	SR 404	Rt 30 to RT 5	8	9.	166	39.9	23	Signal and the state of the sta	49.0	0.0%	-	45	₹
SR 404	SR 404	KI 3 IO KI 3U	AND I	0.	5	1,51		жжиния — — — — — — — — — — — — — — — — — — —					
04	SR 404	RT5 to SR 1	EB	6.3	525	43.1	68	Signat	49.5	12.9%	-	40,50,45,50	A
SR 404	SR 404	SR1toRT5	WB	Ш	455	49.8	3	Signal	50.1	0.5%	-	45,50,40	4
		ani I (M) of (Split) to M) I in	FB	35	3091.0	40.8	272.5		44.8	8.8%			
R 404	SR 404 Total	MD Line to US 13 (Merge) (PM)	WB	35.1	2739.5	46.1	114.0	***	48.1	4.2%			
	4,00	Mendand Chain Los to 25145 Calif	8		512	49.6	3	Signal	49.9	%9.0	-	20	A
SR 16	SR 16	36/16 Split to Maryland State Line	WB	7.1	495	51.3	0		51.3	%0.0	+	50,35	A
						2.50		April 1 Community (Community Community Communi	340	%00	-	25.35.50	٨
SR 16	SR 16	Rt 36 Split to Rt 13	8 8		155	32.1	0	1	32.1	%0.0	-	35,25,40	: ∢
10	2 HG	7(1-5) (0.74-50-50) (1.75-7)			201								
191	SR 16	Rt 13 to Rt 113	83		616	46.6	18	Signal	48.0	2.8%	-	40,25	۷ .
SR 16	SR 16	Rt 113 to Rt 13	WB	8.0	515	55.9	0	-	55.9	0.0%	-	40,50,35	¥.
	.,	THE GIT TO SEE TO		L	878	43.4	13	Signal	44.3	2.6%	-	50,35,25,35,40	4
SK 16	SK 16	Kt 1 (5 (5 SK 50	D W	, r	568	35.9	184	Signal	53.2	32.4%	+	35,25,35,50,40	4
D	01 70	21 13 03 05 C5							***************************************				
SR 16	SR 16	SR 30 to SR 1	83	4.0	324	45.0	28	Signal	49.2	8.5%		50,40,35,40,50	¥ (
SR 16	SR 16	SR 1 to SR 30	WB		580	25.1	46	congestion	27.3	7.8%	-	40,35,40,50	
		Maryland State Line to SR 1	EB		2080.0	45.5	61.0	**	46.8	2.9%			
X 1년	SR 16 Total	SR 1 to Maryland State Line	WB	26.3	2326.5	40.6	229.5	-	45.1	9.9%			
									100	/80 0	7	O II	{
SR 36	SR 36 Total	RT 404 to SR 36/16 Merge	EB	3.6	266	48.7	0		40.7	0.0%	-	50	۷ 4
		SR 36/16 Split to R1 404	ME	-	/07	C'0+	2		200	27.27			
SR 14	SR 14	Maryland State line to Whiteleysburg Rd	83	<u> </u>	463	60.6	0		60.6	%0'0	-	50	ď
SR 14	SR 14	Whiteleysburg Rd to Maryland State line	WB		474	59.1	0		59.1	0.0%	-	50,35	4
3	200 53	Minician Pd to 15 13	83	18	229	29.1	2	Signal	29.2	0.7%	-	25,35,50	В
SR 14	SB 14	US 13 to Whiteleysburg Rd	WB		220	30.2	0		30.2	0.0%		35,25	∢
		***************************************							* 4-4	2000	,	20 GA 02	4
SR 14	SR 14	US 13 to SR 15	8	6.2	421	53.1	0	Western and Jerson William Control of the Control o	33.1	200	-   ,	07,04,05	, ,
SR 14	SR 14	SR 15 to US 13	WB	9	419	53.4	8	Signal	54.4	1.5%		75,40,50,40	
4	SR 14	SR 15 to US 113	EB	1:1	113	36.4	9	Signal	38.5	5.3%	1	40,50	8
SR 14	SR 14	US 113 to SR 15	WB	Ш	85	48.3	2	Signal	49.1	1.8%	-	40,35	۷ ا
4	SR 14	US 113 to SR 1	83	2.1	320	23.2	36	Signal	26.2	11.3%	1	35,25,35,40	В
SR 14	SR 14	SR 1 to US 113	WB		265	28.1	96	Signal	43.9	36.1%	•	35,25,35	ď
			ľ		-	7 77	42 5		45.7	2.8%			
SR 14	SR 14 Total	Maryland State Line to SK 1	n a	19.0	1461 5	46.9	105.0	-	50.5	7.2%			
			2			1	27.7	!					

	SO	∢	¥		В	В		8	٥		∢ `	×	A	A		A	٧	,	<u>.</u>	ť	Ā	<		¥	∢		A	∢		B	ď				٨	∢		В	<u>ی</u>	4	. A	:	A	A		4
Posted	Speed	30,40,50	50.40.30		35,30,40	30,35,45		45,35	45		50,45	45,50	50	50		50	50		50,55	cc'nc	35 30 35 50	00,00,00,00	06,65,00	35,50	50,35		50,35	35,50		35,40,50	40,35				25,35,40,50	50,40,35,25		35,25	35,45	50 45.35	20,22,00	75	90	50	100000000000000000000000000000000000000	25,50
Ju ch	Lanes	-	-		2	2		2	2		-		-	,	-	2	2		2	7 2	-	-	-	1	-		1	ļ		-	-				-	-		-	~	1	- *		+	-		-
Percent	Time in Delay %	2.1%	7600	22.5	12.0%	19.5%		%0.0	16.7%		16.1%	5.7%	0.2%	2 70%	21.12	15.6%	27.6%		4.2%	20.5%	A E0/	9/07	1,8%	7.3%	8.8%		4.1%	4.0%		7.5%	4.4%	C 00/	7.7%	?	0.0%	0.0%		19.3%	14.6%	7600	V.U.70	07.0.22	1.3%	%0.0		14.6%
Mean Peak	Running Speed (mph)	44 R	53.4	1.70	31.4	32.7		32.4	25.3		49.5	48.6	57.1	£2.7	7.70	48.5	52.0		22.6	48.4	407	6,04	47.3	39.4	44.1		44.1	46.6		34.7	35.6	207	45.0	+ 5	81.6	51.6		25.0	26.1	1,1	0.10	7,60	57.8	60.8		47.5
Peak	Delay Source	Jeaning .	Signa		Signal/Congestion/Stop Sign	Signal		44	Signal		Signal	Signal	Cian Cian	igio dos	Signal	Signal	Signal		traffic congestion	Signal		Signal	Signai	Signal/Congestion/Stop Sign	Consultan Sion		Signal	Signal		Signal/Congestion	Signal		###				THE PARTITION OF THE PA	Signaf	Signal	AND THE PROPERTY OF THE PROPER		Signal	Signal	Signar 		Signal
Total Peak	Delay (Seconds)	(Seconds)		0	38	58		0	24		06	29	,	- 5	18	21	41		11	34	-	12	4	30	55	?	13	12	7,	33	19		250.5	2///		C		55	38		o	92	- L	2	5	64
Mean Peak	Travel	fudiu) paade	43.8	52.1	7.70	26.3		32.4	21.1		41.5	45.8	0 11	57.0	51.3	410	37.6		21.7	38.4		38.7	46.3	7 90	50.3	40.4	42.3	7.88		32.1	34.0		39.7	41.9	81.5	21.0	0.15	20.2	22.3		51.6	45.1	57.4	57.1	60.8	40.6
Mean Peak	Travel Time	(Seconds)	339	285	286	866	222	96	144		559	507	1	219	679	135	147		264	149		258	216	****	150	400	314	790	187	442	418		3831.5	3620.5	250	507	ò	284	257		326	374		419	393	442
	Dist. (Miles)	1	**	4.1	2.2	3.2	1 1 1	0.9	0.8		6,4	6.4		2.6	9.7	1 5	2 42		1.6	1.6		2.8	2.8		9.6	ų. 4.	3.7		3.7	3.9	3.9		42.2	42.2	7.3	; r	5.5	1.6	1.6		4.7	4.7		6.6	6.6	5.0
-	<u> </u>		8	MB	l co	a la	170	85	WB	-	83	WB			WB	62	88		69	WB		EB	WB	-	3	WG	g	3 5	aw	83	WB		田	WB	1 02	9 5	GVV	63	WB		囧	WB		8 9	WB	E8
	Segnients		MD State Line to Sussex Ave.	Sussex Ave. to MD State Line	2 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	SUSSEX Ave. 10 US 137 SN 20 VV	US 137 SH ZU W 10 SUSSEX AVE.	115 13 1 SB 30 W to 115 13 1 SB 30 F	115 13 1 SR 20 F to 115 13 1 SR 20 W	101 101 101 101 101 101 101 101 101 101	US 13/20 E merge to US 9	US 9 to US 13/20 E split		US 9 to SR 20 W/US 113 Merge	SR 20 W / US 113 Split to US 9		SK 20 W/US 113 Metge (U SK 24	100 CT 10	SR 24 to SR 20 E/US 113 Split	SR 20 E/US 113 Merge to SR 24	AND	SR 20 E / US 113 Split to SR 26	SR 26 to SR 20 E / US 113 Merge	The state of the s	SR 26 to SR 17	SR 17 to SR 26	Court Na CO at Car Co	agials to the or an analysis	SR 54 split to SR 17	SR 54 Merce to SR 1	SR 1 to SR 54 Split		Maryland State Line to SR 1	SR 1 to Maryland State Line	CONTRACTOR	MU line to Road 499	Road 499 to MU line	Road 499 to US 13	11S 13 to Road 499		US 13 to Road 449	Road 449 to US 13	The state of the s	Road 449 to 30/24 split	30/24 spill to Road 449	30/24 split to US 113
	Route Name		SR 20	SR 20		SR 20	SR 20	00 00	2K 20	20.00	SR 20	SR 20		SR 20	SR 20		SR 20	3K 20	58.20	SR 20		SR 20	SR 20		SR 20	SR 20	25.45	SK 20	SR 20	1 SR 20	SR 20		CD 20 Total	i i i i		SR 24	SR 24	80 GS	20 27	00 67	SR 24	SR 24		SR 24	SR 24	SR 24
	Route		SR 20	SR 20		SR 20	SR 20	20,00	SK 20	2K 2U	SR 20	SR 20		SR 20	SR 20		SR 20	07 XC	SB 20	SR 20		SR 20	SR 20		SR 20	SR 20	4	SH 20	SR 20	VC 00	SR 20		600	4 (5)		SR 24	SR 24	76 00	27 27 20 24	25, 62	SR 24	SR 24		SR 24	SR 24	SR 24

SOT	83	1	n a		<b>₹</b>	۷	1		٤ ا	A	4				۷	. 4		٧	۷		П	m		٨	4	٧	( 6	2			В			С	8		Ą	٧	4	ξ .	٧	٧	∢	
Posted Speed	50,25		25	55,53	50,40,50,35	35,50,40,50		45,50	40	35,40,50,45	50,40,50,35				35	202		40.50	50.40		35,30,35	35,30		40,50,35	35,50.40	35.40	35	Ĉ.			55	55.50		50,55	55		55,50	45	44 44	45,53	45	55,45	55	LLANDON MINISTER CONTRACTOR CONTR
No. of Lanes	+		1	-	-			_	_	-	-			_	-	- -		-	-		+			-	-	•		-			2	-		2	2		2	2	-	7.	2	2	2	-
Percent Time in Delay %	0.0%		16.6%	ZU:07a	9.6%	0.0%		26.2%	0.0%	41.1%	18.7%		19.5%	8.7%	1 200	9000	200	6.8%	0.4%		18.6%	1.3%		9.2%	1.3%	707 407	24 30%	61.370	11.7%	8.1%	18.4%	7004		37.7%	29.9%		8.1%	0.5%		3.6%	21.2%	4.9%	11.7%	1
Mean Peak Running Speed (mph)	33.4		22.5	Z4.U	46.0	47.7		12.3	38.9	44.0	41.9		44.3	44.7		4,10	25.0	55.5	53.8	T	12.6	27.8	-	39.0	47.4		1.1C	20.0	40.2	41.2	1 697	£7.8	5: 72	32.9	40.3		54.6	63.7		46.4	40.6	53.6	53.7	
Peak Delay Source			Signal	Signal	Signal	***		congestion/Signal		Concession/Signal	Signal			u			**************************************	Siros	CON CONTRACTOR	Tigo doto	Signal	Signal		Congestion/Signal	Signal		Signal	Congestion/Signal			A LEGIS	Oginal Comment	Cigital	Signal	Signal		Signal	Signal		Signal	Signal	Cinnal	Cities	12519180
Total Peak Delay (Seconds)	0		25	30	46	0		162	0	757	152	30.	794.5	310.0		0	2	3.7	17	-	88	2		58	9		F .	148	243.5	158.0	445	2 00	97	74	43	î	30	2		3	20	4.5	) <del>`</del>	444
Mean Peak Travel	33.4		18.8	19.2	41.5	47.7		9.0	38.9	0 90	24.4	**	35.6	40.8		51.4	52.6	54.7	21.7	53.0	10.2	27.4		35.4	46.8		41.3	21.1	35.5	37.9	0.0	40.2	54.3	20.5	28.2	20.0	50.2	63.3		44.7	32.0	24.0	0.16	47.4
Mean Peak Travel Tinio	536		151	148	458	398		619	144	7.00	550	010	4081.7	3565.0		231	226	000	300	3/4	474	177		630	477		354	694	2076.5	1947.3		cla	436	197	***	144	372	295		69	95	250	346	372
Dist. (Miles)	5.0		0.8	9.0	5.3	53	?	1.6	1.6	,		7	40.4	40.4		3.3	3.3		3.0	5.6	1.3	13	?	6.2	6.2		4.1	1.4	20.5	20.5		6.9	6.9	* 1	:		5.2	5.2	3.5	0.9	9.0		4.9	2.0
ă.	MB.		E9	ew	83	M/A		E3	WB			I MB I	EB	WB		8	WB	-	£ !	WB	EB	ğ	O.A.	EB	WB		EB	WB	<u> </u>	WB		73	SB	a	3	E C	SB	2		8S	en En		es :	NB
Seyments	US 113 to 30/24 solit		US 113 to SR 30	SR 30 to US 113	SR 30 to SR 5 South	01 02 02 02 02 02 02 02 02 02 02 02 02 02	SA 30 SUBILITY OF SA	SR 5 South to SR 23 / SR 5 North	SR 23 / SR 5 North to SR 5 South	THE PARTY OF THE P	SR 23 / SR 5 North to SR 1	SR 1 to SR 23 / SR 5 North	Maryland State I ine to SR 1	SR 1 to Maryland State Line		SR 54 split to SR 30	SR 30 to SR 54 split	The state of the s	SR 30 to US 113	US 113 to SR 30	11 <u>\$ 113</u> to SR 20	20 20 20 24 25	24 Z0 10 US 1 153	SR 20 to SR 17	SR 17 to SR 20		SR 17 to SR 1	SR 1 to SR 17	SD 54 Split to SB 1	SR 1 to SR 54 Split		SR 24 to SR 54 (MD Line)	SR 54 (MD Line) to SR 24	10 03 11 11 W 0 03	#7 NG 01 18 AV 02 NG	SR 24 to SR 9 West	SR 20 East to SR 9 West	CO DIAMAGE IN CO DO DE CO	ST 3 VESI IO ON EVICENSI	SR 20 West to SR 20 East	SR 20 East to SR 20 West		SR 404 E to SR 20 West	SR 20 West to SR 404 E
Route Name	SR 24	-315	SR 24	SR 24	Ac do	47 US	SK 24	SR 24	SR 24		SR 24	SR 24		Total		SR 26	SR 26		SR 26	SR 26	80.00	27.50	SK 26	SR 26	SR 26		SR 26	SR 26		SR 26 Total		US 13	US 13		US 13			2 22		US 13	US 13		1	US 13
Route	2E 34	200	SR 24	SR 24	74 00	47 70	SR 24	SR 24	SR 24		SR 24	SR 24		SR 24 Total		SR 26	SR 26	Ì	SR 26	SR 26	50 00	27.50	SR 26	58.26	SR 26		SR 26	SR 26		SR 26		US 13 Dover	US 13 Dover	<i>t</i>	US 13 Dover	US 13 Dover	155 13 Chyer	CO CO CO	US 13 Dover	US 13 Dover	US 13 Dover		US 13 Dover	US 13 Dover

Transal Time         Transal Time         Doblay         Doblay         Spended (mph)         Doblay (mp)			-		Mean reak						7	Doctor	-
Secretary Secretary   Secretary Secretary Secretary Secretary Secretary   Secretary Secretar	알	Segments	ä	Dist. (Miles)	Travel Time (Seconds)	Travel Speed (mph)	Delay (Seconds)	Delay Source	Running Speed (mph)	Time in Delay %	Lanes	Speed	SOI
Secretive Secretive   Sign	ı									1,12		44	ţ
Since the District Name	1	SR 404 W to SR 404 E	88	2.5	455	19.8	175	Signal	32.1	38.5%	7	CC	، ر
Since the Since of the Since of the Since of Sin	1	SR 404 E to SR 404 W	2	2.5	195	46.7	15	Signal	50.6	7.7%	2	99	₹
Since Set No. 1967   Since Set No. 1971   Signature Set No. 1971   Signature Set No. 1974   Since Set No. 1974   Signature Set No. 1974   Signat		AMARINE STATE AND STATE					ľ	1	59.7	3,69,5	2	35.55	A
SR 14 to SR 16 SR 16 SR 16 SR 18 3.3 122 SR 15 SR 10 S		SR 16 to SR 404 W	SB	3.3	234	50.3	5	Signal	36.2	2,07,2	, ,	55.45.35	. ✓
STATE   STAT		SR 404 W to SR 16	E E	3.3	232	51.1	13	Juga 2		2			
Section 10   Section 11   Sec		20 44 to 00 44	87	8.2	436	67.8	0	***	67.8	%0.0	2	45,50,55,45,35	4
SR 1 LOS STATE STATES STATE STATES ST		D: NO 01 41 NO	3 2	6 8	207	59.8	0		59.8	0.0%	2	55,50,45	∢
SRY 12 6 SPY		0K 18 (0 UK 14	- I	2.0	-			The state of the s					
SR 100 BR		SR 12 to SR 14	SB	5.8	638	32.5	110	Congestion/Construction/Signal	39.2	17.2%	2	55,45,35	<b>a</b>
SR TO LOSE RELACED SER 10A		SR 14 to SR 12	B	5.8	367	56.6	0		56.6	%0.0	2	45,50,55,45	4
SR 12 6 SR 10 SR 1		William							F 2.7 4	14 00/	,	55 65 55 55 65 55	٨
SRT 12 D SRT 10. M SRT 10.	_	SR 10A to SR 12	SB	4.5	323	50.6	39	Signai	37.4	2000	2 0	85 55	: 4
SR 10 to SR 10A GR 10 LB 11 LB 12A GR	6	SR 12 to SR 10A	2	4.5	304	53.4	0		33.4	0/00	*	70,01	
SR 10 to S		VOY 63 -1 07 93	a/	0.5	307	35.5	43	Signal	41.3	14.0%	2	50,55	Ð
SR 264 (MD State Line)	'n	ANI NO DI NO	3 5		330	45.2	8	Signal	46.7	3.1%	2	55,50	В
SR 10 to US 13 US 113 Split to SR 26 (MD State Line)	m	SR 10A to SR 10	S	3.0	503	3.55	,						
SR 64 (MD State Line) to US 13 / US 110 State Line) to US 13 / US 113		1 00 -1 10 440 D-13 4- D-10 40	as	3.5	414	31.6	82	Congestion/Signal	39.3	19.7%	2	50	æ
US 31 ULS 113 Split to SR S4 (MD State Line) to Columbia R4 to R4020   A916	2	01 No 01 110 01 121 00	5 2	2	423	30.7	43	Signal	34.2	10.2%	2	50,35	ខា
SR 64 (MD State Line)		SK 10 to US 13 / US 13 Merge	Q.	5	031				-				
SR 54 (MD State Line) to US 13 / US 113 Merge   NB   49,8   3611.0   49,6   214.0		US 13 / US 113 Split to SR 54 (MD State Line)		49	4402.0	40.7	693.0		48.4	15.7%			
Manydard Line to Columbia Rd to Waller Rd (RD 512) to Columbia Rd (RD 512)	Ē	SR 54 (MD State Line) to US 13 / US 113 Merge		49	3611.0	49.6	214.0		52.8	5.9%			
Columbia Red Line Re Columpia Red Maydard Line Re Columpia Red Maydard Line Re Columpia Red Maydard Line Red Columpia Red Maydard Line Red Columpia Red (RD 512) to LS 13 to RD 512 to RD 512 to LS 13 to RD 512		1. Call 1. T. Call 1. T. Call 1. Call		ţ	76	44.8	c		55.8	0.0%	-	50	4
Columbia Rd to Manyland Line         WB         1.2         77         55.2         0         —         55.2         0         —         55.2         0         —         55.2         0         —         55.2         0         —         55.2         0         —         55.2         0         —         55.2         0         —         55.2         0         —         55.2         0         —         55.2         0         —         55.2         0         7         40.25         1         55.2         0         —         55.2         0         —         55.2         0         —         55.2         0         —         55.2         0         —         55.2         0         —         55.2         0         —         55.2         0         —         55.2         0         —         55.2         0         —         55.4         1         25.40         1         25.40         1         25.40         1         25.40         1         25.40         1         25.40         1         25.40         1         25.40         1         25.40         1         25.40         1         25.40         1         25.40         1         25.40 <td>4</td> <td>Maryland Line to Columbia Kd</td> <td><u>a</u></td> <td>7.1</td> <td>2 1</td> <td>2.5</td> <td>,</td> <td>LECTO</td> <td>57.2</td> <td>1.3%</td> <td>-</td> <td>50.40</td> <td>٨</td>	4	Maryland Line to Columbia Kd	<u>a</u>	7.1	2 1	2.5	,	LECTO	57.2	1.3%	-	50.40	٨
Columbia Rd (RD 512) to US 13 to Waller Rd (RD 512) to US 13 to Walle	z.	Columbia Rd to Maryland Line	WB	1.2	77	56.5	-	Signal	2.16	0.5.1		21.00	
Waller Rd (FD 512) to Columbia Rd         Waller Rd (FD 512) to Columbia Rd         FD 52         Congestion/Signal         15.1         22.8%         1         40.25           Waller Rd (FD 512) to Columbia Rd         Waller Rd (FD 512) to Columbia Rd         Waller Rd (FD 512) to Columbia Rd         4         5.62         4         Signal         15.1         22.8%         1         22.8%         1         25.40         1           US 13 to Waller Rd (FD 512)         WB         1.3         165         2.62         3         Signal         15.8         1         25.40         1         25.40         1         25.40         1         25.40         1         25.40         1         25.40         1         25.40         1         25.40         1         25.40         1         25.40         1         25.40         1         25.40         1         25.40         1         25.40         1         25.50         1         25.50         1         25.50         1         25.50         1         25.50         1         25.50         1         25.50         1         25.50         1         25.50         1         25.50         1         25.50         1         25.50         1         25.50         2         25.50<	[2	Columbia Rd to Maller Rd (RD 512)	EB .	5.0	331	55.0	0	1	55.0	0.0%	1	50	٨
Walter Rd (RD 512) to US 13         EB         1.3         399         11.6         91         Congestion/Signal         15.1         22.6%         1         25.40           US 13 to Walter Rd (RD 512) to US 13 to US	,   z	Waller Rd (RD 512) to Columbia Rd	₹	5.0	330	55.2	0	***	55.2	0.0%	-	40,25	A
Waller Rd (RD 512) to US 13 to Waller Rd (RD 512)   WB		THE PROPERTY OF THE PROPERTY O						ALL PROPERTY OF THE PROPERTY O			1	44.44	ť
US 1310 Waller Rd (RD 512)   WB   1.3   165   28.2   4   Signal   28.6   2.1%   1   25.35.0	8	Waller Rd (RD 512) to US 13	8		336	11.6	91	Congestion/Signal	15.1	22.8%	-	25,40	2 0
MD 353 Merge to MD 353 Merge to MD 353 Merge to MD 353 Merge to MD 353 Split to US 13 to MD 353 merge to SR 26 Split to US 113 to SR 26 Split to US 26 Split to	4	US 13 to Waller Rd (RD 512)	WB	1,3	165	28.2	**	Signai	28.8	2.1%		00,00,02	2
MD 353 Spirit bu S 13 Spirit bu S	,	AND THE PROPERTY OF THE PROPER	ä		572	56.2	3	Signal	58.5	0.5%	-	35	۲
MD 353 merge to SR 26 Split         EB         2.4         163         52.0         0          52.0         0.0%         1         35.50.35           SR 26 Merge to MD 353 Split         WB         2.4         165         51.5         6         Signal         53.3         3.3%         1         35.50.35           SR 26 Split to US 113 to SR 26 Split         EB         8.4         641         47.2         11         Signal         47.9         1.6%         1         35.25           US 113 to SR 26 Split         WB         8.4         606         49.9         2         Signal         50.0         0.3%         1         35.25           US 113 to SR 26 Split         EB         1.1         129         29.6         5         Signal         30.8         1         25.35           SR 17 to US 113         WB         1.1         134         28.5         15         Signal         44.6         2.9%         1         50.35.25.35.03.55.03           SR 17 to US 113         MB         1.3         5.2         43.4         15         Signal         44.6         2.9%         1         35.50.35.20.35.03.60.70		MD 353 Shift to 15 13	N N		657	48.9	92	Signal	55.8	13.9%	-	50,35	4
MD 353 merge to SR 26 Split         EB         2.4         163         52.0         0          52.0         0.0%         1         35,30,33           SR 26 Merge to MD 353 Split         WB         2.4         165         51.5         6         Signal         53.3         3.3%         1         35           R 26 Split to US 113 to SR 26 Split         WB         8.4         64.1         47.2         11         Signal         47.9         1.6%         1         35.25           US 113 to SR 26 Split         WB         8.4         606         49.9         2         Signal         50.0         0.3%         1         35.25           US 113 to SR 26 Split         WB         1.1         129         29.6         5         Signal         30.8         3.9%         1         35.25           WB         1.1         134         28.5         15         Signal         31.9         10.8%         1         50.3%         1         50.35.25.50.36.25           SR17 to US 113         WB         1.1         134         28.5         15         Signal         44.6         2.9%         1         50.35.25.35.03.40												7. C. 7. F.	ŕ
SR 26 Merge to MD 353 Split         EB         84         641         47.2         11         Signal         47.9         1.6%         1         35         1         35         1         35         1         35         1         35         1         35         1         35         35         1         35	54	MD 353 merge to SR 26 Split	留	2	163	52.0	0	***	52.0	0.0%		32,00,03	,
SR 26 Split to US 113 to SR 27 Split         EB         8.4         606         49.9         2         Signal         47.2         16%         1         35.25           US 113 to SR 17 to US 113         WB         1.1         129         29.6         5         Signal         30.8         3.9%         1         25.35           SR 17 to US 113         WB         1.1         134         28.5         15         Signal         31.9         10.8%         1         25.35           SR 17 to US 113         WB         1.1         134         28.5         15         Signal         31.9         10.8%         1         25.35           SR 17 to US 113         WB         1.1         134         28.5         15         Signal         44.6         2.9%         1         50.35.25.35.50.35.25           SR 17 to SR 20         EB         6.3         520         43.4         15         Signal         44.6         2.9%         1         35.50.35.25.35.50.40	75	SR 26 Merge to MD 353 Split	WB	2	165	51.5	9	Signal	53.3	6.5.5		75	
SRT7 to SR 20   EB   C3   C3   C3   C3   C3   C3   C3   C		CD 25 CAR to 115 413	EB	8.4	641	47.2	11	Signal	47.9	1.6%	1	35	K
US 113 to SR 17 to US 113 to SR 20 EB 6.3 520 43.4 15 Signal 44.6 2.9% 1 5.50.35.50.40 EB 6.3 5.20 43.4 15 Signal 42.5 0.5% 1 35.50.35.50.40	g	כון פס מו ווולפ פס עפ	3 5		505	40 0	2	Sional	50.0	0.3%		35,25	⋖
US 113 to SR 17         EB         1.1         129         29.6         5         Signal         30.8         3.9%         1         25.35           SR 17 to US 113         WB         1.1         134         28.5         15         Signal         31.9         10.8%         1         25.35           SR 17 to US 113         WB         1.1         134         28.5         15         Signal         44.6         2.9%         1         50.35.25.35.50.35.25           SR 17 to SR 20         EB         6.3         5.3         5.2         47.3         3         Slop Sign         42.5         0.5%         1         35.50.35.53.50.40	, l	US 113 to SR 26 Split	200		200	25.5	4	,				, , , , , , , , , , , , , , , , , , ,	
SR 17 to US 113 WB 1.1 134 28.5 15 Signal 31.9 10.8% 1 25.35	15	11S 113 to SR 17	83	Ĺ	129	29.6	22	Signai	30.8	3.9%	+	25,35	ď
SR 17 to SR 20 EB 6.3 520 43.4 15 Signal 44.6 2.9% 1 50.35.25.35,50.35,25 and a second state and a second st	. I	3.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5	2/5/2	Ľ	134	28.5	15	Signal	31.9	10.8%	-	25,35	А
SR 17 to SR 20 EB 6.3 520 43.4 15 Signal 44.6 2.9% 1 50.35.25.35.50.35.25 ASS 20.35.50 ASS 20.35	×	SR 17 to US 113	GAS	╛	5	5.53							
Slop Sign 42.5 0.5% 1 35,50,35,25,35,50,40	54	SR 17 to SR 20	EB	L	520	43.4	15	Signal	44.6	2.9%	-	50,35,25,35,50,35,25	
CD 3112 CB 17	:   1	71 82 91 68 82	N N		533	42.3	3	Stop Sign	42.5	0.5%	-	35,50,35,25,35,50,40	_

FOS				ď	٨		٨	4		A	٨	٥	•		٧	٧		٨	٨		4	4	Ţ	٠	4				٧	٧		٨	4	A	4					∢	4	۲	۵	c 	٨	
Posted	Speed			55	55		55	55		55	55	1.1	CC.	CC	55	55		55	55		55	55	11 10 00 11 11 11	55,40,25,55	55,40,25,55				55,50	50		50	50	50 35 50	20,25,25					55	65	7.5	93	20	65	
No. of	Lanes		1	2, 3, 2	2.3.2		3,2	2		4, 2, 3	2, 3, 2		3.4	o, e, c	4.3	5.4		4	4		3,4	4		3	4.3									-						2,3	3,2	٥	5 6	٠	3	}
Percent		4.4%	4.5%	0.0%	H	1	0.0%	%0.0		-	11.9%	120	0.0%	0.0%	%0.0	%0.0		%0.0	%0.0		%0.0	0.0%		18.4%	6.0%	,000	3.0%	2.3%	%0.0	%0.0		%0.0	%0.0	769.0	780 4	8,0,0	%0.0	2.5%		0.0%	0.0%	7000	0.0%	0.0%	0.0%	
<u>×</u>		45.9	48.9	53.5	56.6	The state of the s	61.3	56.1		65.8	65.2	1	48.7	53.8	59.0	61.7		74.3	71.9		76.7	73.6	<u> </u>	64.1	49.7		64.4	62.0	57.2	51.0		57.9	58.6	527	25.7	4750	55.3	57.5	=======================================	71.2	59.7		72.2	66.1	69.2	
Peak	Delay Source	***	1			*	4.7			1	Accident/ Right lane closed		-			++,	MANAGEMENT CONTRACTOR			Management of the second of th	1	***		Toll Congestion	Toll Congestion		****	-	_	1	THE TAXABLE PROPERTY OF THE PR			***************************************	10:30 = 1 H	ioil Congestion		***	r			***************************************	***			
Total Peak	Delay (Seconds)	124.5	120.5	c			0	0		0	19		0	0	0			0	0		0	0		30	Ξ		29.8	29.3	C			0	0		0	8	0.0	0 6	2'0	0	a		0	0	0	
Mean Peak	Travei Speed (mph)	43.9	46.7	52.5	0.00	0.00	61.3	56.1		65.8	57.4	7	48.7	53.8	0 03	517		74.3	71.9		7.6.7	73.6		52.3	46.7		62.4	60.2	57.9	54.0		57.9	58.6	1	52.7	59.6	55.3	56.5	90.1	71.2	59.7		72.2	66.1	69.2	
Mean Poak	Travel Time (Seconds)	┢	2665.0	00	60	64	54	58	3	152	156		7.4	99	10,	12.7		63	99	3	201	209		162	178		977.8	995.3	123	130	501	78	75		171	149	3718	262 8	202.0	103	111		48	51	78	
Piet	(Miles)	34.5	34.5	-	? .	1.3	6.0		2.0	2.8	2.5		1.0	1.0		2 6	3.0	1.3	-	2	4.3	4.3		2.3	2.3		17.0	16.6	9.5	2.0	2.0	1.3	1.2	2	2.5	2.5	47	, r	-	2.0	1.8		1.0	6.0	1.5	_
<u> </u>	늄		WB		2 1	I as	MB	9	25	SN NB	a.	1	SB.	SB	1	2 5	1 20 1	l BR	8	as I	S.	SB	-	NB NB	SB		98	SB	00	9 9		83	wB		EB	WB	ū	3 2 2	WD	NBN	SB		8N	SB	a a	
	Segments	MD State Line to SR 20	SR 20 to MD State Line		Exit 7 (Defaware Ave) to Exit 8	Exit 8 to Exit 7 (Delaware Ave)	Est 6 (Manufact Ave.) to Est 7	CALC (Malylatin Ave) to CAL	EXIL / 10 EXIL 0 (Maryland Ave)	L405 ICT to Evit 6 (Maryland Ave)	Exit 6 (Manufact Ave) to 1.005 101	EXIL O (VIOLITIES AVE.) 10 1-104 AVE.	Exit 5 (SR 141/1-295 JCT) to 1-495 JCT	1-495 JCT to Exit 5 (SR 141/1-295 JCT)	***************************************	Exit 4 (SR 1/Churchmans) to Exit 5 (1-295)	F285 to Exit 4 (SR 1/Churchmans)	Evil 3 (SR 273) to Evil 4 (SR 1)	1 10 10 10 10 10 10 10 10 10 10 10 10 10	EXI( 4 (SK 1) 10 EXI( 3 (SK 2/3)	Exit 1 (SR 896) to Exit 3 (SR 273)	Exit 3 (SR 273) to Exit 1 (SR 896)		MD Line to Exit 1 (SR 896)	Exit 1 (SR 896) to MD Line	THE RESERVE THE PROPERTY OF TH	MD State Line to SR 20	SR 20 to MD State Line	THE SALE OF SA	1-95 to US 13	US 13 to 1-95	11S 13 to SR 9	SR 9 to US 13		SR 9 to D.M.B.	D.M.B. to SR 9	0 88 0 24 30 1	191 O D.W.D	D.M.B to I-95	1.05 to Exit 1 (US 13)	Exit 1 (US 13) to 1:95	THE REPORT OF THE PROPERTY OF	Exit 1 (US 13) to Exit 2 (Rt 9)	Exil 2 (Rt. 9) to Exil 1 (US 13)	F 19-12 410 307 6 11-12	EAR C 11% of 16 LAN O
	Route Name		SR 54 Total		1-95	1-95	10.	28-1	1-95	96-	50-1	CS-	1-95	1-95		1-95	1-95	301	26-1	1-95	503	1-95		56-1	1:95					1-295	1-295	1.205	1-295		1-295	1-295		I-295 Total		207	1495		1-495	1-495	3011	1483
	Route		SRS		1-95	1-95	10.	Se-1	1-95	30.1	000	CS-	1.95	1.95		1-95	1-95	#01	CR-I	1-95	1.05	-05	70-1	1.05	1-95		-	<u> </u>		1-295	1-295	306.1	1-295		1-295	1-295		1-29		1 405	282		1-495	1495		1880

SOT	⋖	4	A		∢ .	4	m	¥				В	4	A	A	-			٨	V V	A	4		∢ .	∢	60	A	4	8			<u> </u>			A	٨		۷.	٧
Posted Speed	65	25	65	***************************************	65	Ç	65	65				45	42	35	35				35,50	35,50	40.50.35.25	40,50,35,25		50,35,25	50,35,25	90	50	40	40	74 44 44	23,40,30	25,40,50			20	50		35,50	35,50
No. of Lanes	3	٤.	E	,	т ;	2,3	3,2	2	-			+	-	2	2				-	-	-	-		1	-	-	-	-	-	-	- -	_			-			1	-
Percent Time in Delay %	%0.0	%00	0.0%		0.0%	0.0%	0.0%	0.0%	760 0	%0.0	22.22	13.7%	%0.0	45.5%	0.0%	702.00	24.1.70	0.07%	12.4%	20.8%	2.3%	4.7%		%0.0	%0.0	4.5%	%0.0	17.6%	11.2%		0.0%	3.7%	4.7%	6.1%	0.2%	1 9%		%0:0	0.0%
Mean Peak Running Speed (mph)	Н	647	62.5		73.2	69.1	49.8	70.0	58 5	85.8 85.8	2500	39.7	43.8	33.4	38.8	, 33	38.1	42.0	45.5	43.7	38.1	38.6		47.8	52.7	42.6	52.3	37.2	35.4		39.3	42.5	42.1	44.3	57.2	57.2		43.2	41.5
Poak Delay Source						***		_				Signal	1	Signal					Signal	Stop Sign	legois	Signal				Yield Sign		Signal	Signal		***	Signal/Yield Sign	***	1	Signal	Sing Sing	180 400		1
Total Peak Delay (Seconds)	0				0	0	0	0	00	0.0	0.0	35.0	0:0	63.0	0.0		99.0	0.0	27.0	52.0	1. F.	24.0	A:	0.0	0.0	10.0	0.0	33.0	20.5		0.0	6.5	81.5	103.0	10	5.5	0.23	0.0	ç
Mean Peak Travel Speed (mph)	64.2		62.5		73.2	69.1	49.8	70.0	1 00	68.5	02.0	34.3	43.8	18.2	38.8		28.7	42.6	39.8	34.6	27.2	26 A	7.55	47.8	52.7	40.6	52.3	30.6	31.5		39.3	40.9	40.1	41.6	57.1	37.1	1.00	43.2	
Mean Peak Travel Time (Seconds)	H		£ 6	Ò	240	252	72	55	0 000	623.U	030.3	262.5	205.5	138.5	65.0		401.0	270.5	217.0	249.5	2 (1)2	502.5	2,000	429.5	389.5	221.5	172.0	188.0	183.0		183.0	176.0	1741.5	1678.5	7 31.3	030.7	D40.U	125.0	
Dist. (Miles)	15		<u>.</u> .	-	4.9	4.8	1.0	1.1	- 9 1	11.8		2.5	2.5	0.7	0.7		3.2	3.2	2.4	2.4	5	3.6	3.5	5.7	5.7	2.5	2.5	1.8	1.6		2.0	2.0	19.4	19.4		2 2	é	1.5	
i i	SB		2 0	25	NB	SB	NB	SB	L	9 6		SB	BN BN	BS	E S		SB	NB	SB	NB	-	200	ON:	SB	NB NB	85	8	BS	g R		SB	SN N	SB	Ω <sub>N</sub>	g	0 9	SN NB	SB	
Segments	Exit 3 to Exit 2 (Rt. 9)	WHAT ARE THE TAXABLE PROPERTY OF TAXABLE P	Exit 3 to Exit 4 (Rt. 3 Marsh Rd.)	EXIL4 (Rt. 5 Melsis Rt.) to Exis 5	Exit 4 (Marsh Rd.) to Exit 5 (Rt. 13)	Exit 5 (Rt. 13) to Exit 4 (Marsh Rd.)	Exit 5 (US 13) to PA Line	PA Line to Exit 5 (US 13)		1-95 (DE) to 1-95 (PA Line)	1-95 (PA Line) to 1-95 (DE)	US 9 to SR 24	SR 24 to US 9	SR 24 to SR 1	SR 1 to SR 24		US 9 to SR 1	SR 1 to US 9	SR 1 to SR 16	SR 16 to SR 1	A ALL EAT AND	9 X 15 10 US 3	0.3 9.10 5K 10	US 9 to SR 23	SR 23 to US 9	CD 23 to CD 24 Culii	SR 24 Spit to SR 23	S Solit in SR 24 Memo	SR 24 Merge to SR 24 Split	**************************************	SR 24 Merge to Indian River Bay	Indian River Bay to SR 24 Merge	SR 1 to Indian River Bay	Indian River Bay to SR 1	CF 311 - 32 LO : F3 LO	SR 54 / SR 25 to US 13	US 13 to SR 54 / SR 26	SR 54 Merge to SR 54 / SR 26	The state of the s
Route Name	1-495		1-495	1-483	1-495	1-495	1-495	1495		1-495 Total		Plantation Rd.	Plantation Rd.	Da noitetacio	Plantation Rd.		SP 40 Total	i constant	SRS	SRS		SRS	SK5	SR5	SRS	203	SR5	900	SR5		SR 5	SR 5		SR 5 Total		SR 30	SR 30	SR 30	
Route	1495		1-495	- C641	1-495	1-495	1405	1495		1495		SR 1D	SR 1D	20 10	SR 1D		SD 41	45	SRS	SRS		SRS	SRS	SR 5	SR 5	3 03	SRS	1 00	SRS		SR 5	SR 5		SR		SR 30	SR 30	SR 30	***************************************

Wilsolaria (Seconds)         Speed (mph) (Seconds)         Colay         Running (Speed (mph) (Seconds))         Travel Time (Travel Time (Seconds))         Travel Time (Seconds)         Travel Time (Seconds)					-	Mean Peak	Mean Peak	Total Peak	Peak	Mean Peak	Percent	No. of	Posted	
3.3         219.0         54.2         0.0%         1         35.50           3.3         222.0         53.5         0.0         -         53.5         0.0%         1         35.50           0.9         55.7         58.2         0.0         -         58.5         0.0%         1         55.0           0.9         60.5         55.7         58.6         0.0         -         53.6         0.0%         1         50           5.0         60.5         55.7         55.6         0.0         -         48.9         0.0%         1         50           6.0         372.0         48.4         5.5         519nal         24.6         32.0%         1         55.0           6.0         372.0         48.4         5.5         519nal         24.6         32.0%         1         25.50           6.0         138.0         21.2         40.0         51.8         24.6         32.0%         1         25.50           6.8         138.0         22.1         51.0         51.0         51.0         23.0%         1         40.45.50           8.4         582.0         372.0         52.0         51.0         51.0	Route Name Segments Dir.		ä			Travel Time	Travel	Delay (Seconds)	Delay	Running Speed (mph)	Time in Delav %	Lanes	Speed	3
3.3         219.0         54.2         0.0          54.2         0.0%         1         35.50           3.3         222.0         53.5         0.0          53.5         0.0%         1         35.50           0.9         55.7         58.2         0.0          50.6         1         50           0.9         60.5         53.6         0.0          53.6         1         50           5.0         361.0         48.4         5.5         0.0          53.6         1         50           5.0         372.0         48.4         5.5         Signal         24.5         1.5%         1         25.50           6.0         172.0         16.7         55.0         Signal         21.8         2.3%         1         25.50           8.4         582.0         27.2         21.0         Signal         53.9         1         40.45.50           8.4         582.0         52.0         21.0         Signal         53.9         1         40.45.50           8.4         582.0         52.3         32.7         Signal         53.9         1         40.45.50				4	-	(enumpac)	apear (upus)	(2000)						
3.3         222.0         53.5         0.0         —         53.5         0.0%         1         36.50           0.9         522.0         53.6         0.0         —         53.6         0.0%         1         50           0.9         60.5         53.6         0.0         —         53.6         0.0%         1         50           5.0         372.0         48.4         5.5         Signal         48.1         1.5%         1         55           6.0         372.0         48.4         5.5         Signal         24.6         32.0%         1         25.50           6.0         17.2         55.0         Signal         24.6         32.0%         1         25.50           8.4         54.7         55.6         Signal         55.8         3.3%         1         25.50           8.4         54.7         55.6         Signal         53.9         3.6%         1         40.45.50           8.4         56.7         4.0         Signal         53.9         3.6%         1         40.45.50           8.4         56.7         4.0         5.0         3.3%         1         40.45.50           8.4	SO CANADAM CAN		30	L		219.0	54.2	0.0	**************************************	54.2	0.0%	1	35,50	٧
0.9         55.7         58.2         0.0         -         58.2         0.0%         1         50           0.9         55.7         53.6         0.0         -         53.6         0.0%         1         50           5.0         381.0         48.4         5.5         0.0         -         49.9         0.0%         1         25.50           5.0         372.0         48.4         5.5         Signal         24.6         32.0%         1         25.50           0.8         172.0         16.7         55.0         Signal         24.6         32.0%         1         25.50           0.8         136.0         21.2         4.0         Signal         24.6         32.0%         1         25.50           8.4         582.0         22.0         21.0         Signal         55.8         1         40.45.50           8.4         582.0         22.0         21.0         Signal         55.9         1         40.45.50           8.4         582.0         52.0         21.0         Signal         53.4         2.2%         1         40.45.50           8.5         52.0         40.5         Signal         53.2 <t< td=""><td>SN 20 Weige to SN 24 Meres</td><td></td><td>2</td><td><math>\perp</math></td><td></td><td>222.0</td><td>53.5</td><td>0.0</td><td></td><td>53.5</td><td>0.0%</td><td>1</td><td>35,50</td><td>4</td></t<>	SN 20 Weige to SN 24 Meres		2	$\perp$		222.0	53.5	0.0		53.5	0.0%	1	35,50	4
6.9         55.7         58.2         0.0         -         58.2         0.0%         1         50           6.05         53.6         0.0         -         53.6         0.0%         1         50           5.0         361.0         48.9         0.0         -         49.9         0.0%         1         50           5.0         372.0         48.4         5.5         Signal         24.6         32.0%         1         25.50           0.8         172.0         16.7         4.0         Signal         24.6         32.0%         1         25.50           0.8         136.0         21.2         4.0         Signal         24.6         1.5%         1         25.50           8.4         543.7         55.6         1.7         Signal         53.9         1         40.45.50           8.4         582.0         22.0         53.9         35.8         1         40.45.50           8.4         582.0         52.0         51.0         Signal         53.4         1         40.45.50           8.4         582.0         52.3         8.0         13.5         1         40.45.50           8.5         530.7 <td></td> <td></td> <td></td> <td>1</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>***</td> <td></td>				1									***	
5.0         60.5         5.3.6         0.0         —         53.6         0.0%         1         50           5.0         361.0         48.4         5.5         Signal         —         49.9         0.0%         1         25.50           5.0         372.0         48.4         5.5         Signal         24.6         1.5%         1         25.50           0.8         172.0         16.7         5.0         Signal         24.6         1.6%         1         25.50           0.8         136.0         21.2         4.0         Signal         21.8         2.9%         1         25.50           8.4         582.0         21.0         21.0         Signal         55.8         1         40.45.50           8.4         582.0         27.0         21.0         Signal         53.9         3.6%         1         40.45.50           5.4         406.0         47.5         32.7         Signal         53.4         2.2%         1         40.45.50           5.4         372.0         47.6         15.0         Signal         53.4         2.2%         1         40.45.50           8.2         55.0         47.6         10.0	SS and St.		BS	_		55.7	58.2	0.0	***************************************	58.2	%0.0	-	95	4
5.0         361.0         48.9         0.0         —         49.9         0.0%         1         25.50           5.0         372.0         48.4         5.5         Signal         49.1         1.5%         1         25.50           0.8         172.0         16.7         55.0         Signal         24.6         32.0%         1         25.50           0.8         136.0         21.2         4.0         Signal         21.8         2.3%         1         40.45.50           8.4         54.3         55.6         1.7         Signal         52.9%         1         40.45.50           8.4         582.0         21.0         Signal         52.1         8.0%         1         40.45.50           8.4         582.0         47.9         32.7         Signal         52.1         8.0%         1         40.45.50           8.5         5.4         372.0         52.3         8.0         Signal         52.1         8.0%         1         40.45.50           8.2         560.7         52.0         13.7         Slop Sign/Signal         51.2         2.3%         1         40.50           8.2         560.7         50.0         13.5	SR 26 Merge to SR 24 Split		E E	<u>_</u>	6.0	60.5	53.6	0.0	_	53.6	0.0%		50	A
5.0         301.0         49.3         5.5         Signal         49.1         1.5%         1         25.50           5.0         372.0         16.7         55.0         Signal         24.6         32.0%         1         25.50           0.8         172.0         16.7         55.0         Signal         21.8         2.9%         1         25.5           0.8         136.0         21.2         4.0         Signal         55.8         0.3%         1         40.45.50           8.4         582.0         52.0         21.0         Signal         52.3         1         40.45.50           5.4         372.0         47.6         13.7         Signal         52.1         8.0%         1         40.45.50           8.2         582.0         52.3         8.0         Signal         53.4         22%         1         40.45.50           8.4         372.0         52.3         8.0         Signal         53.4         22%         1         40.50           8.2         560.7         47.6         15.0         Signal         51.2         23%         1         40.50           8.2         560.7         50.0         13.7 <td< td=""><td></td><td></td><td>-</td><td></td><td></td><td>-</td><td>0.07</td><td></td><td></td><td>6.67</td><td>0.0%</td><td>-</td><td>25.50</td><td>4</td></td<>			-			-	0.07			6.67	0.0%	-	25.50	4
5.0         372.0         48.4         5.5         Signal         49.1         1.5%         1         25.0           0.8         172.0         16.7         55.0         Signal         24.6         32.0%         1         25           0.8         136.0         21.2         4.0         Signal         21.8         2.9%         1         25           8.4         543.7         55.6         1.7         Signal         55.8         0.3%         1         40.45.50           5.4         406.0         47.9         32.7         Signal         52.1         8.0%         1         40.45.50           5.4         372.0         52.3         8.0         Signal         52.1         8.0%         1         40.45.50           8.2         55.3         36.7         1         40.45.50         1         40.45.50           8.4         560.7         52.3         8.0         Signal         53.4         2.2%         1         40.45.0           8.2         560.7         50.0         13.7         Stop Sign/Sign/Signal         46.8         2.4%         1         40.50           8.2         50.5         1         40.50         -	SR 30 US 113 to SR 24 Split SB		S	_	5.0	301.U	48,8	0.0				-	CH NC	
0.8         172.0         16.7         55.0         Signal         24.6         32.0%         1         25           0.8         136.0         21.2         4.0         Signal         21.8         25%         1         25           8.4         543.7         55.6         1.7         Signal         55.8         0.3%         1         40.45.50           8.4         582.0         52.0         21.0         Signal         52.1         6.0%         1         40.45.50           5.4         406.0         47.9         32.7         Signal         52.1         6.0%         1         50           5.4         372.0         52.3         8.0         Signal         53.4         22%         1         50           8.2         59.7         50.0         13.7         Stop Sign/Signal         51.2         2.3%         1         40.50           8.2         590.7         50.0         13.7         Stop Sign/Signal         51.2         2.4%         1         40.50           8.2         620.5         47.6         15.0         51.0         52.2         3.3%         1         40.50           43.6         3143.0         49.9	SR 30 SR 24 Spit to US 113 NB		BN BB		5.0	372.0	48.4	5.5	Signal	49.1	1.5%	-	Ac'cz	
0.8         136.0         21.2         4.0         Signal         21.8         2.9%         1         25           8.4         543.7         55.6         1.7         Signal         55.8         0.3%         1         40,45.50           8.4         562.0         52.0         21.0         Signal         53.9         3.6%         1         40,45.50           5.4         406.0         47.9         32.7         Signal         52.1         8.0%         1         40,45.50           5.4         372.0         52.3         8.0         Signal         53.4         2.2%         1         50           8.2         590.7         50.0         13.7         Stop Sign/Signal         51.2         2.2%         1         40,50           8.2         620.5         47.6         15.0         Stop Sign/Signal         48.8         2.4%         1         40,50           43.6         3143.0         49.9         65.5         -         52.2         33%         -         40,50	S		SS	_	0.8	172.0	16.7	55.0	Signal	24.6	32.0%	-	52	۲
543.7         55.6         1.7         Signal         55.8         0.3%         1         40,45.50           562.0         52.0         21.0         Signal         53.9         3.6%         1         40,45.50           406.0         47.9         32.7         Signal         52.1         6.0%         1         50           550.7         50.0         13.7         Slop Sign/Signal         51.2         2.3%         1         40,50           620.5         47.6         15.0         Slop Sign/Signal         48.8         2.4%         1         40,50           3143.0         49.9         65.5         -         52.2         3.3%         -         40,50	US 113 to SR 24 Merge		NB NB	1	0.8	136.0	21.2	4.0	Signal	21.8	2.9%	-	25	<u> </u>
593.7         53.0         1.7         Signal         53.9         3.6%         1         40.45.50           406.0         47.9         32.7         Signal         52.1         8.0%         1         50           372.0         52.3         8.0         Signal         53.4         2.2%         1         50           590.7         50.0         13.7         Stop Sign/Signal         51.2         2.3%         1         40.50           620.5         47.6         15.0         Stop Sign/Signal         48.8         2.4%         1         40.50           3143.0         49.9         65.5         -         51.0         2.1%         1         40.50						1	G 41	4.7	Cario	555	0.3%	-	40,45,50	\\
8.4         582.0         52.0         21.0         Signal         52.1         8.0%         1         50           5.4         406.0         47.9         32.7         Signal         52.1         8.0%         1         50           8.2         55.0         52.3         8.0         Signal         53.4         2.2%         1         50           8.2         590.7         50.0         13.7         Stop Sign/Signal         48.8         2.4%         1         40.50           43.6         3109.7         50.5         104.0          52.2         3.3%          40.50           43.6         3143.0         49.9         65.5          51.0         2.1%          51.0	SR 30 US 9 to SR 24 Marge		2	4	5	345.7	0.00	7.7	1	0.63	3 607	+	60.45.50	٩
5.4         406.0         47.9         32.7         Signal         52.1         6.0%         1         50           5.4         372.0         52.3         8.0         Signal         53.4         22%         1         50           8.2         590.7         50.0         13.7         Stop Sign/Signal         48.8         2.4%         1         40.50           8.2         620.5         47.6         15.0         Stop Sign/Signal         48.8         2.4%         1         40.50           43.6         3143.0         49.9         65.5         -         51.0         51.0         2.1%	SR 30 SR 24 Merge to US 9 NB		92		8.4	582.0	52.0	23.0	olgnas	20.2	2,00	-	222.12	-
5.4         372.0         52.3         8.0         Signal         53.4         2.2%         1         50           8.2         590.7         50.0         13.7         Stop Sign/Signal         51.2         2.3%         1         40.50           8.2         620.5         47.6         15.0         Stop Sign/Signal         48.8         2.4%         1         40.50           43.6         3143.0         50.5         104.0          52.2         3.3%         1           43.6         3143.0         49.9         65.5          51.0         2.1%         1	8S 6 SI (49) 8S		S	1	5.4	406.0	47.9	32.7	Signal	52.1	8.0%	1	50	V
8.2         590.7         50.0         13.7         Slop Sign/Signal         51.2         2.3%         1         40.50           8.2         620.5         47.6         15.0         Slop Sign/Signal         48.8         2.4%         1         40.50           43.6         3109.7         50.5         104.0          52.2         3.3%         3.3%           43.6         3143.0         49.9         65.5          51.0         2.1%	US 9 to SR 16		2	<u></u>	5.4	372.0	52.3	8.0	Signal	53.4	2.2%	-	50	∢
8.2         590.7         500         13.7         Stop Sign/Signal         31.2         2.3%         1         40.50           8.2         620.5         47.6         15.0         Stop Sign/Signal         48.8         2.4%         1         40.50           43.6         3109.7         50.5         104.0          52.2         3.3%           43.6         3143.0         49.9         65.5          51.0         2.1%		THE PROPERTY OF THE PROPERTY O							1 27 17		ç,	,	40 50	۷
8.2         620.5         47.6         15.0         Stop Sign/Signal         48.8         2.4%         1         40.50           43.6         3169.7         50.5         104.0          52.2         3.3%            43.6         3143.0         49.9         65.5          51.0         2.1%	SR 30 SR 1 to SR 16 SB		BS		8.2	590.7	50.0	13.7	Stop Sign/Signal	31.2	6.578	- -	20.00	٠,
43.6         3109.7         50.5         104.0          52.2           43.6         3143.0         49.9         65.5          51.0	SR 30 SR 16 to SR 1 NB		N	H	8.2	620.5	47.6	15.0	Stop Sign/Signal	48.8	2.4%	-	46,50	٤
43.6     3109.7     50.5     104.0      52.2       43.6     3143.0     49.9     65.5      51.0										3	7000			-
43.6 3143.0 49.9 65.5 - 51.0	SR 1 to US 13			SB	43.6	3109.7	50.5	104.0		7.76	5.5%			
	SR 30 Total US 13 to SR 1	US 13 to SR 1		NB.	43.6	3143.0	49.9	65.5		51.0	2.1%			-

### **Total Peak Travel Time Data Summer 2008**

Dist. Miles	Mean Peak	Mean Peak	Total Peak	Peak	Mean Peak	Percent
	Travel Time	Travel	Delay	Delay	Running	Time
	(Seconds)	Speed (mph)	(Seconds)	Source	Speed (mph)	in Delay %
1168.8	95811	43.9	8072	**	48.0	8.4%

### Delaware Center for Transportation University of Delaware Newark, Delaware 19716

### AN EQUAL OPPORTUNITY/AFFIRMATIVE ACTION EMPLOYER

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